

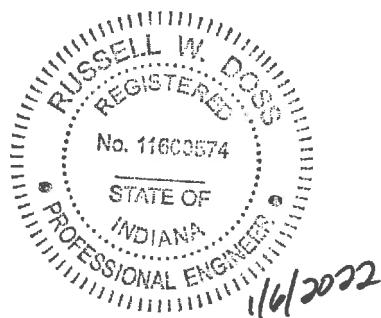
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DOLLAR GENERAL Time 9:30 AM Initials AR  
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EVANSVILLE, IN

## DRAINAGE REPORT



Prepared By:

 **Overland**  
ENGINEERING, LLC  
1598 IMPERIAL CENTER SUITE 2009  
WEST PLAINS, MISSOURI 65775  
PH 417-256-8150

**DOLLAR GENERAL  
EVANSVILLE , IN**

**DRAINAGE REPORT**

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**I. INTRODUCTION**

DGOGEvansvillein10202021 LLC proposes to construct a 10,640 sq ft Dollar General Store on a 1.98 acre site in the Vanderburgh County just west of Highway 57 on Boonville-New Harmony Road. The project will add 40,570 s.f. of impervious area to the property. This drainage report details the impact of the project on storm water runoff and the detention design intended to address runoff concerns.

**II. CERTIFICATION**

This report was prepared by Overland Engineering, LLC, under the direction of Russell W. Doss, Indiana Professional Engineer No. 11600574.

**III. DESIGN SUMMARY**

The proposed Dollar General project will add approximately 0.93 acres of pavement and building to the existing 1.98 acre undeveloped property. Without control measures, the increase in impervious area will create a corresponding increase in peak runoff as indicated detailed in calculations included in Appendix IX.

Per Vanderburgh County requirements, the rational runoff equation has been used to estimate peak rates of runoff and required detention volume for the proposed project.

As the watershed map in Appendix XI indicates, there is no offsite runoff contributing to the detention basin and runoff analysis. A total of 1.34 acres drains to the detention basin. This area contains all new impervious area proposed for the project.

Other than the Rule 5 land disturbance requirements, no state or federal permits are required for the project.

A dry detention basin has been chosen as the method to control increased peak flow from the proposed project. Runoff from all developed onsite areas will drain to the detention basin where post-project peak runoff from the 25-year storm event will be limited to the 10-year pre-project peak flow rate. This peak reduction is accomplished through storage of 4,758 c.f. of runoff and flow restriction through a circular orifice. A riprap emergency spillway has also been designed to pass the fully developed 100-year peak flow.

Per the calculations in Appendix IX, 4,266 c.f. of detention volume is required for peak flow control. Adding 10% for sedimentation, the total required volume is 4,700 c.f. The storage volume provided in conjunction with the 5" orifice at elevation 391.00 restricts peak runoff for the 25-year design storm to 0.75 cfs. The 25-year design stage corresponding to 4,758 c.f. of storage is elevation 392.22. The 6' emergency spillway has been set at elevation 393.25 (12" above design elevation), and will pass the 100 year peak developed flow at elevation 393.85. The 100 year stage of 393.85 is also more than 2.0 feet fellow the finished floor elevation of 396.00.

The primary reference used in the calculations is Chapter 13.04 of Vanderburgh County Code.

**IV. DESIGN CRITERIA**

As noted above, the applicable design criteria for the proposed storm water detention facility is the return period of 25 years.

**V. TIME OF CONCENTRATION**

Time of concentration values for pre-project and post-project conditions were calculated to be 14 minutes and 5 minutes, respectively. The calculations are detailed on Form 830 included in Appendix V. Exhibits showing the pre-project and post-project flow paths used for time of concentration calculations are also included in Appendix V.

**VI. ALLOWABLE DISCHARGE & STORAGE VOLUME**

The allowable discharge for the proposed project is 0.75 cfs as indicated by calculations included in Appendix IX. Per County requirements, the allowable discharge is based on the 10-year pre-project peak flow, with no reduction due to downstream inadequacy or other permit conditions.

There are no developed areas that leave the site undetained.

A summary of the detention volume calculations are included in Appendix VI and in Appendix IX.

**VII. NOT USED**

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**VIII. OUTLET STRUCTURE**

Discharge for the design storm is controlled by a 5" circular orifice at elevation 391.00, connected to the outlet pipe. A 6' wide riprap emergency overflow spillway is provided at elevation 393.25 and conveys the 100-year post-project peak flow without allowance for the 5" orifice. Maximum 100-year stage in the emergency overflow is at elevation 393.85.

**IX. DETENTION**

The maximum design ponding depth in the detention basin is 1.22 feet (392.22-391.00) and provides 4,758 c.f. of storage volume. At the design elevation of 392.22, 12 inches of freeboard is provided below the spillway elevation of 393.25

Stage-Storage-Discharge plots for the detention basin are included in Appendix IX.

The required detention volume for peak flow control is 4,266 c.f. Per the requirement to add 10% of the volume for sedimentation, the total required volume is 4,700 c.f.

The proposed finished floor elevation is 396.00, while the proposed 100-year stage in the detention basin is 393.85. This meets the 2 foot separation requirement.

The overflow riprap spillway (elev 393.25) will convey the 100-year peak developed flow of 7.22 cfs at a depth of 0.60 feet (elev 393.85). This assumes the low flow orifice is inoperable.  $Q = 2.7 * 6 * (0.6)^{1/2} = 7.52 \text{ cfs}$ .  $V = 7.52 \text{ cfs} / 3.0 \text{ s.f.} = 2.5 \text{ ft/sec.}$

Both the low-flow orifice and the riprap overflow spillway will function with little or no maintenance. In the event the 5" orifice becomes clogged, the emergency spillway will convey the required flow with no danger of malfunction. The 5" low-flow can be cleared by simply removing the obstruction.

Seeding of the detention basin floor will be per specifications on Sheet C3.1, and will be maintained equivalent to a residential lawn. The side slopes of the detention basin will be sodded per Sheet C3.

The bottom of the detention basin is sloped between 0.50% and 1.0% slope.

**X. STORM SEWERS & CHANNELS**

One grate inlet on the west side of the building collects runoff from the west parking lot (14,958 s.f.). Total 100-year peak flow to the grate inlet is calculated as 3.02 cfs. Assuming a clogging factor of 50%, the inlet has a capacity of 3.09 cfs. The inlet will accept the 100-year peak flow rate assuming it is 50% clogged.

A 15" RCP running at 0.50% slope connects this inlet to the detention basin. The pipe has a full capacity of 4.95 cfs. The 15" RCP will convey the 100-year peak runoff from the north parking lot and building to the detention basin.

Similary, the east channel drains 15,560 s.f. of impervious area from the west parking lot. The total 100-year peak flow to the channel is calculated as 3.27 cfs. The west side channel has a base width of 2 feet, side slopes of 4:1, a maximum depth of 1 foot, and a longitudinal slope of 0.8%. As a grass channel, roughness is assumed at 0.038. At a depth of 0.46 feet, the channel will carry 3.27 cfs. The east side channel has adequate capacity to convey the 100-year peak flow to the detention basin. Velocity is calculated at 1.8 feet per second.

Calculations for the storm sewer and channel are located in Appendix X.

**XI. DRAINAGE PLAN DRAWINGS**

Drawings of the proposed project are included in Appendix XI. They include the ALTA survey, Site Plan – C1, Grading Plan – C2, Drainage Details – C2.1, Erosion Control Plan – C3, Erosion Control Details – C3.1 & C3.2, and Landscaping Plan – C4.

The watershed map and soil map are also included in Appendix XI.

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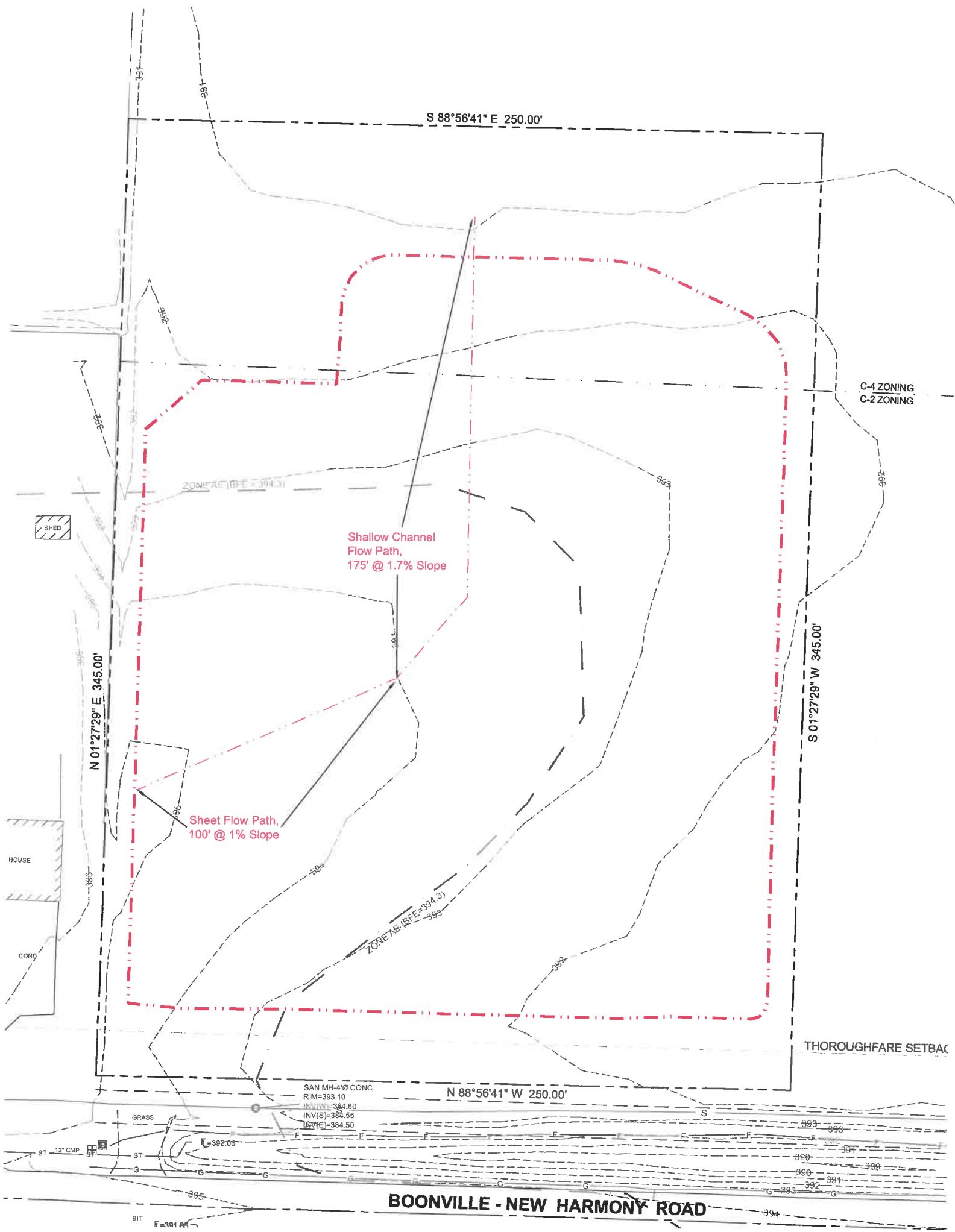
## **APPENDIX V**

## Pre-Project

### Section V

*Form 830 Note: Include a map, schematic or description of flow segments*

Sheet Flow (Applicable to Tc Only)	Segment ID		
1. Surface description	Sheet		
2. Manning's roughness coefficient, n			
3. Flow length, L (total $L \leq 300$ ft)	(ft)	.15	
4. Two-year 24-hour rainfall, P <sub>2</sub>	(in)	100	
5. Land slope, s	(ft/ft)	3.3	3.3
6. $T_t = \frac{0.007(nL)^{0.8}}{P_2^{0.5}S^{0.4}}$	Compute T <sub>t</sub>	(hr)	.212
Shallow Concentrated Flow	Segment ID	Shallow	
7. Surface description (paved or unpaved)			
8. Flow length, L	(ft)	175	
9. Watercourse slope, s	(ft/ft)	.017	
10. Average velocity, V	(ft/s)	2.1	
11. $T_t = \frac{L}{3600 V}$	Compute T <sub>t</sub>		.0231
Channel Flow	Segment ID		
12. Cross sectional flow area, a	(ft <sup>2</sup> )		
13. Wetted perimeter, P <sub>w</sub>	(ft)		
14. Hydraulic radius, r = $\frac{a}{P_w}$	Compute r	(ft)	
15. Channel slope, s	(ft/ft)		
16. Manning's roughness coefficient, n			
17. $V = \frac{1.49 r^{2/3} s^{1/2}}{n}$	Compute V	(ft/s)	
18. Flow length, L	(ft)		
19. $T_t = \frac{L}{3600 V}$	Compute T <sub>t</sub>	(hr)	
20. Watershed or subarea T <sub>c</sub> or T <sub>t</sub> (add T <sub>t</sub> in steps 6, 11, and 19) (hours)			.235
(Note P <sub>2</sub> for Vanderburgh County-use 3.3)			

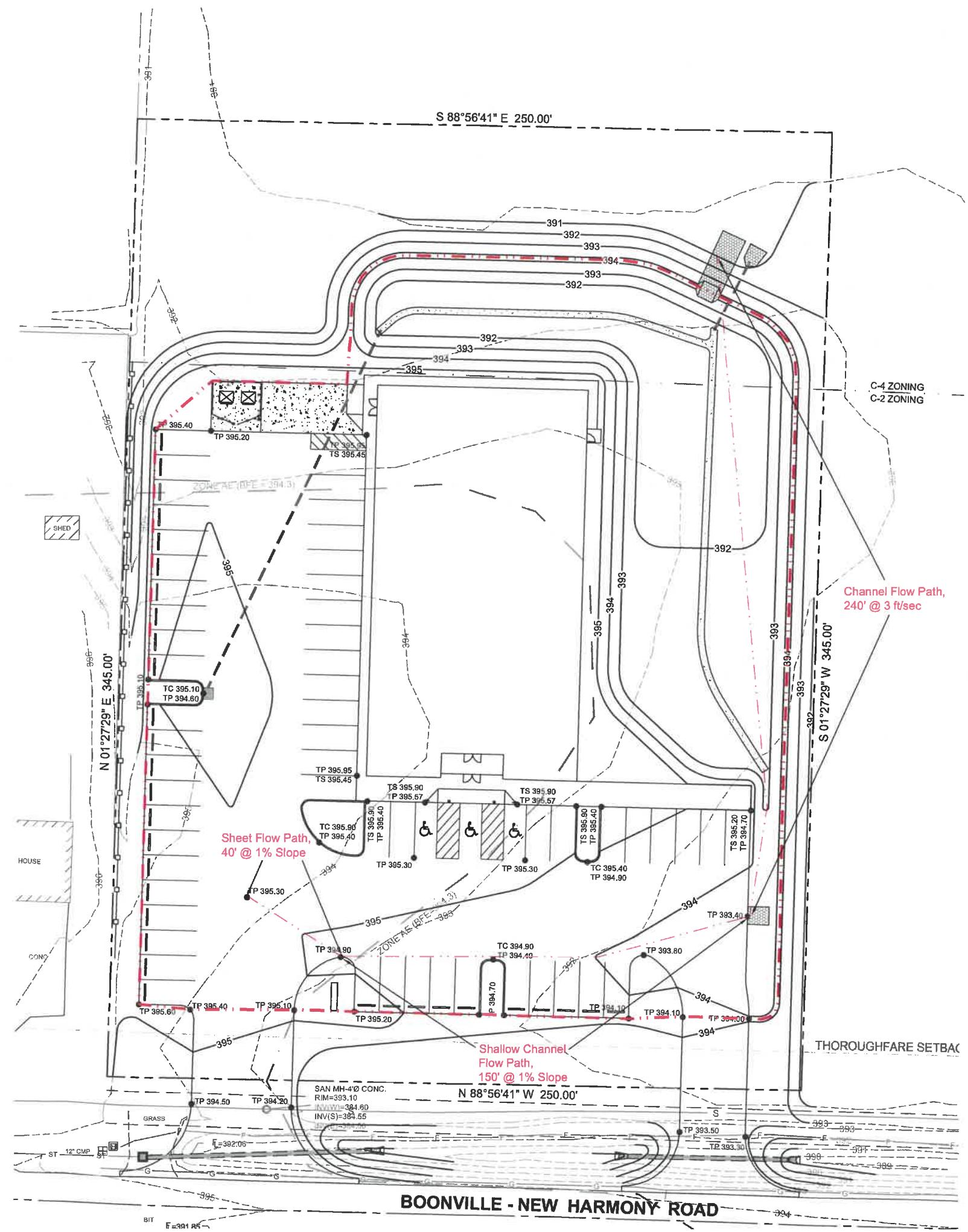


## Post-Project

### Section V

*Form 830 Note: Include a map, schematic or description of flow segments*

Sheet Flow (Applicable to Tc Only)	Segment ID	
1. Surface description	Sheet	
2. Manning's roughness coefficient, n		
3. Flow length, L (total $L \leq 300$ ft)	(ft)	.011
4. Two-year 24-hour rainfall, P <sub>2</sub>	(in)	40
5. Land slope, s	(ft/ft)	3.3
6. $T_t = \frac{0.007(nl)^{0.8}}{P_2^{0.5}s^{0.4}}$	Compute T <sub>t</sub>	(hr) .01
		.0126
Shallow Concentrated Flow	Segment ID	Shallow
7. Surface description (paved or unpaved)		
8. Flow length, L	(ft)	150
9. Watercourse slope, s	(ft/ft)	.01
10. Average velocity, V	(ft/s)	2.00
11. $T_t = \frac{L}{3600 V}$	Compute T <sub>t</sub>	.0208
		.0208
Channel Flow	Segment ID	Channel
12. Cross sectional flow area, a	(ft <sup>2</sup> )	2.5
13. Wetted perimeter, P <sub>w</sub>	(ft)	7.123
14. Hydraulic radius, r = $\frac{a}{P_w}$	Compute r	(ft) .351
15 Channel slope, s	(ft/ft)	.01
16. Manning's roughness coefficient, n		.037
17. $V = \frac{1.49 r^{2/3} s^{1/2}}{n}$	Compute V	(ft/s) 2.00
18. Flow length, L	(ft)	240
19. $T_t = \frac{L}{3600 V}$	Compute T <sub>t</sub>	(hr) .0333
20. Watershed or subarea T <sub>c</sub> or T <sub>t</sub> (add T <sub>t</sub> in steps 6, 11, and 19) (hours)		.0667
(Note P <sub>2</sub> for Vanderburgh County-use 3.3)		



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## APPENDIX VI

<b>Section VI-Calculation of Undeveloped C</b>			
<b>Form VIa</b>	<b>Watershed</b>	<b>Onsite - Pre</b>	
	C	Area	C x A
Surface Type-Woodland, Turfed Meadows, Rough Pasture, Fallow Brush			
Less than 2%	0.12	<u>1.34</u>	<u>.16</u>
2% to 5%	0.24	_____	_____
5+% to 10%	0.36	_____	_____
Over 10%	0.48	_____	_____
Surface Type-Cultivated Fields			
Less than 2%	0.2	_____	_____
2% to 5%	0.35	_____	_____
5+% to 10%	0.5	_____	_____
Over 10%	0.65	_____	_____
Surface Type-Pavement, Rooftop, Other Impervious Surfaces:			
Less than 2%	0.92	_____	_____
2% to 5%	0.94	_____	_____
5+% to 10%	0.96	_____	_____
Over 10%	0.98	_____	_____
Surface Type-Lawns with turf			
Less than 2%	0.15	_____	_____
2% to 5%	0.25	_____	_____
5+% to 10%	0.40	_____	_____
Over 10%	0.55	_____	_____
Gravel Roadway or Parking (10 year storm)	0.5	_____	_____
Water/Lake	1.00	_____	_____
Other (Provide Reference)_____	_____	_____	_____
<b>TOTAL</b>		<u>1.34</u>	<u>.16</u>
<b>Weighted Undeveloped C</b>			<u>.12</u>

<b>Section VI-Calculation of Developed C</b>			
<b>Form VIb</b>	<b>Watershed</b>	<b>Onsite - Post</b>	
	<b>C</b>	<b>Area</b>	<b>C x A</b>
Surface Type-Woodland, Turfed Meadows, Rough Pasture, Fallow Brush			
Less than 2%	0.12	_____	_____
2% to 5%	0.24	_____	_____
5+% to 10%	0.36	_____	_____
Over 10%	0.48	_____	_____
Surface Type-Cultivated Fields			
Less than 2%	0.2	_____	_____
2% to 5%	0.35	_____	_____
5+% to 10%	0.5	_____	_____
Over 10%	0.65	_____	_____
Surface Type-Pavement, Rooftop, Other Impervious Surfaces:			
Less than 2%	0.92	<u>.93</u>	<u>.856</u>
2% to 5%	0.94	_____	_____
5+% to 10%	0.96	_____	_____
Over 10%	0.98	_____	_____
Surface Type-Lawns with turf			
Less than 2%	0.15	<u>.41</u>	<u>.062</u>
2% to 5%	0.25	_____	_____
5+% to 10%	0.40	_____	_____
Over 10%	0.55	_____	_____
Gravel Roadway or Parking			
(25 year storm)	0.6	_____	_____
(50 & 100 year storm)	0.65	_____	_____
Water/Lake	1.00	_____	_____
Other _____ (Provide Reference for C Value)	_____	_____	_____
TOTAL		<u>1.34</u>	<u>.918</u>
Weighted Developed C			<u>.69</u>

**FORM 800**

Watershed ID	Onsite				
Allowable Outflow Rate	0.75 cfs				
Area	1.34 acres				
Developed C	0.69				
Detention Facility Design Return Period (25, 50 or 100)	25				
Rainfall Intensity	Inflow Rate	Outflow rate	Storage Rate	Storage Required (acre-ft)	Storage Required (cubic ft)
25      50      100					
5      7.81      8.82      9.95	7.22	0.75	6.47	.045	1941
10     6.32     7.13     8.05	5.84	0.75	5.09	.070	3054
15     5.24     5.92     6.68	4.84	0.75	4.09	.085	3681
20     4.43     5.00     5.64	4.10	0.75	3.35	.092	4020
25     3.80     4.29     4.84	3.51	0.75	2.76	.095	4140
30     3.31     3.73     4.21	3.06	0.75	2.31	.095	4158
40     2.58     2.91     3.29	2.39	0.75	1.64	.090	3936
45     2.31     2.61     2.94	2.14	0.75	1.39	.086	3753
50     2.08     2.35     2.65	1.92	0.75	1.17	.081	3510
60     1.95     2.23     2.56	1.80	0.75	1.05	.087	3780
90     1.67     1.94     2.25	1.54	0.75	0.79	.098	4266
120    1.37    1.59    1.84	1.27	0.75	0.52	.086	3744
180    1.02    1.18    1.37	0.94	0.75	0.19	.047	2052
240    0.82    0.95    1.11	0.76	0.75	0.01	.003	144

**DOLLAR GENERAL**  
**EVANSVILLE , IN**

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## APPENDIX IX

DOLLAR GENERAL #24125  
 HYDRAULIC CALCS  
 BY: Overland Engineering LLC  
 Date: 1/6/2022

Rational Method, Q = CIA

**Pre Project**

**TR 55 Method**

**Sheet Flow**

Flow length 100 ft  
 Land slope 0.01 ft/ft  
 Manning's n 0.15 Short Grass  
 2 yr/24hr rainfall 3.3 in

t = 12.7 min

**Shallow concentrated flow**

Flow length 175 ft  
 Slope 0.017 ft/ft  
 Avg. velocity 2.10 ft/s  
 Unpaved t = 1.4 min

**Open channel flow**

Flow length 0 ft  
 Avg. velocity 2.0 ft/s  
 t = 0.0 min

Tc = 14.1

**Post Project**

**TR 55 Method**

**Sheet Flow**

Flow length 40 ft  
 Land slope 0.01 ft/ft  
 Manning's n 0.011 Pavement  
 2 yr/24hr rainfall 3.3 in

t = 0.8 min

**Shallow concentrated flow**

Flow length 150 ft  
 Slope 0.01 ft/ft  
 Avg. velocity 2.03 ft/s  
 PAVED t = 1.2 min

**Open channel flow**

Flow length 240 ft  
 Avg. velocity 2.0 ft/s  
 t = 2.0 min

Tc = 4.0

Tc (total) = 14.00 min

Tc (total) = 5.00 min (use 5 minute min.)

Intensity z= 3.51 in/hr

Intensity 10= 4.65 in/hr

**Weighted Runoff C**

C <sub>1</sub> =	0.94	Paved Areas
A <sub>1</sub> =	0.00	
c <sub>2</sub> =	0.12	Grass/Lawns
A <sub>2</sub> =	1.34	

Drain Area Total = 1.34 acres

C (composite) = 0.12

Q<sub>2</sub> = 0.56 cfs

Q<sub>10</sub> = 0.75 cfs

#### Detention Volume Provided

CONIC VOLUME			
Water Surface Elevation ft (input)	Corresponding Contour Area square feet (input)	Volume above Datum acre-ft (output)	Volume above Datum Cubic Feet (output)
391.0	0	0.000	0
392.0	5.748	0.066	2,874
393.0	11.377	0.263	11,437

#### Required Storage Elevation with 10% Additional for Sedimentation

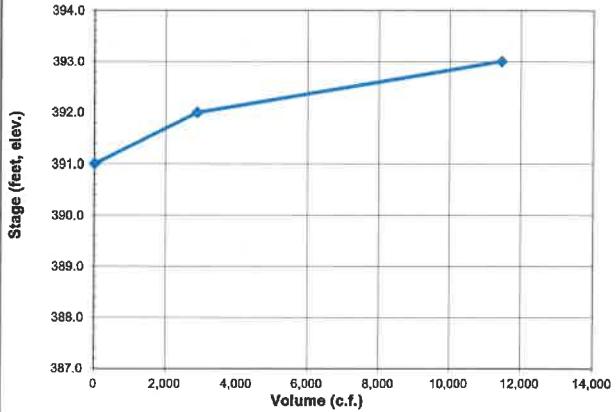
ELEV<sub>10</sub> = 392.22 ft Total Volume = 4758 c.f.

#### Outlet Structure Design

##### Inputs

Low Flow		Weir 1
5" Orifice @ 391.21		
	cfs	
391.00	0.00	L = 6.00
391.50	0.35	C <sub>w</sub> = 2.70
391.75	0.48	E <sub>o</sub> = 393.50
392.00	0.58	
392.25	0.67	
392.50	0.74	
392.75	0.81	
393.00	0.88	
393.25	0.94	
393.50	0.99	
Janning's n-values		
		PVC 0.012
		PE (<9"dia) 0.015
		PE (>12"dia) 0.02
		PE(9-12"dia) 0.017
		CMP 0.024
		ADS N12 0.012
		CMP 0.024
		Conc 0.013

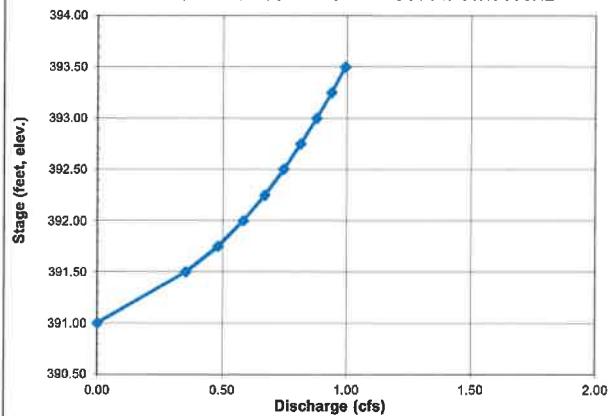
#### STAGE-VOLUME CURVE FOR THE DETENTION BASIN



#### Rating Curve of Outlet Structure

Elevation	Q1	Q2	Resulting Flow
	Low Flow cfs	Weir Flow cfs	
391.00	0.00	0.00	0.00
391.50	0.35	0.00	0.35
391.75	0.48	0.00	0.48
392.00	0.58	0.00	0.58
392.25	0.67	0.00	0.67
392.50	0.74	0.00	0.74
392.75	0.81	0.00	0.81
393.00	0.88	0.00	0.88
393.25	0.94	0.00	0.94
393.50	0.99	0.00	0.99

#### STAGE-DISCHARGE CURVE FOR THE OUTLET STRUCTURE



#### Compare Outflow Elevation to Required Storage Elevation

Max Outflow cfs	Occurs at Elevation	Required Elevation	At or above req.?
Q <sub>10 allowable</sub> = 0.75	392.51	392.22	YES

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## **APPENDIX X**

S 88°56'41" E 250.00'

C-4 ZONING  
C-2 ZONING

SHED

N 01°27'29" E 345.00'

HOUSE

CONO

TP 394.50 TP 394.20

SAN MH-4' CONC.  
RIM=393.10  
INV(W)=394.60  
INV(S)=394.55  
INV(R)=394.50

N 88°56'41" W 250.00'

BOONVILLE - NEW HARMONY ROAD

F=381.85

G=392.06

H=392.06

I=392.06

J=392.06

K=392.06

L=392.06

M=392.06

N=392.06

O=392.06

P=392.06

Q=392.06

R=392.06

S=392.06

T=392.06

U=392.06

V=392.06

W=392.06

X=392.06

Y=392.06

Z=392.06

A=392.06

B=392.06

C=392.06

D=392.06

E=392.06

F=392.06

G=392.06

H=392.06

I=392.06

J=392.06

K=392.06

L=392.06

M=392.06

N=392.06

O=392.06

P=392.06

Q=392.06

R=392.06

S=392.06

T=392.06

U=392.06

V=392.06

W=392.06

X=392.06

Y=392.06

Z=392.06

S 01°27'29" W 345.00'

THOROUGHFARE SETBACK

**Dollar General  
12100 SR57  
Inlet and Storm Sewer Calculations  
January 6, 2022**

Runoff to Grate Inlet

Area = 14,958 s.f. = 0.343 acres  
Impervious Area = 14,281 s.f. (C=0.92)  
Lanscaped Area = 677 s.f. (C=.15)  
Composite C = .885  
Tc = 5 minutes (minimum)  
100-year intensity = 9.95 in/hr

$$Q_{100} = 0.885 * 0.343 * 9.95 = 3.02 \text{ cfs}$$

Grate Inlet Capacity – Deeter #2230 (234 in<sup>2</sup>)

$$Q_{100} = 3.02 \text{ cfs}$$

Max depth = 395.10 - 394.60 = 0.5'

$$Q = C * A * (2g * d)^{0.5} = 0.67 * (234/144) * (64.4 * 0.50)^{0.5} = 6.18 \text{ cfs}$$

50% CF \* 6.2 = 3.09 cfs > 3.02 cfs

Capacity of 15" Pipe from Inlet to Detention

$$Q = 1.486 / n * A * R^{2/3} * S^{1/2}$$

n = 0.012

$$A = 3.14/4 * (1.25)^2 = 1.227 \text{ s.f.}$$
$$R = 1.25/4 = 0.313'$$
$$S = .005 \text{ ft/ft}$$
$$Q = 1.486 / .012 * 1.227 * (.313)^{2/3} * (.005)^{1/2}$$
$$= 4.95 \text{ cfs} > 3.02 \text{ cfs}$$

**Dollar General  
12100 SR57  
East Side Channel Calculations  
January 6, 2022**

Runoff to East Side Channel

Area = 15,560 s.f. = 0.357 acres

all impervious (C=0.92)

Tc = 5 minutes (minimum)

100-year intensity = 9.95 in/hr

$$Q_{100} = 0.92 * 0.357 * 9.95 = 3.27 \text{ cfs}$$

Capacity of East Side Channel

Bottom = 2'

4:1 Side Slopes

Depth = 0.46'

Slope = 1.0%

N=0.037

$$Q = 1.486 / n * A * R^{2/3} * S^{1/2}$$

A = 1.79 s.f.

P = 5.83'

$$R = 1.79/5.83 = 0.31'$$

$$Q = 1.486 / .037 * 1.79 * (.31)^{2/3} * (.01)^{1/2}$$

$$= 3.27 \text{ cfs}$$

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## APPENDIX XI

S 88°56'41" E 250.00'

C-4 ZONING  
C-2 ZONING

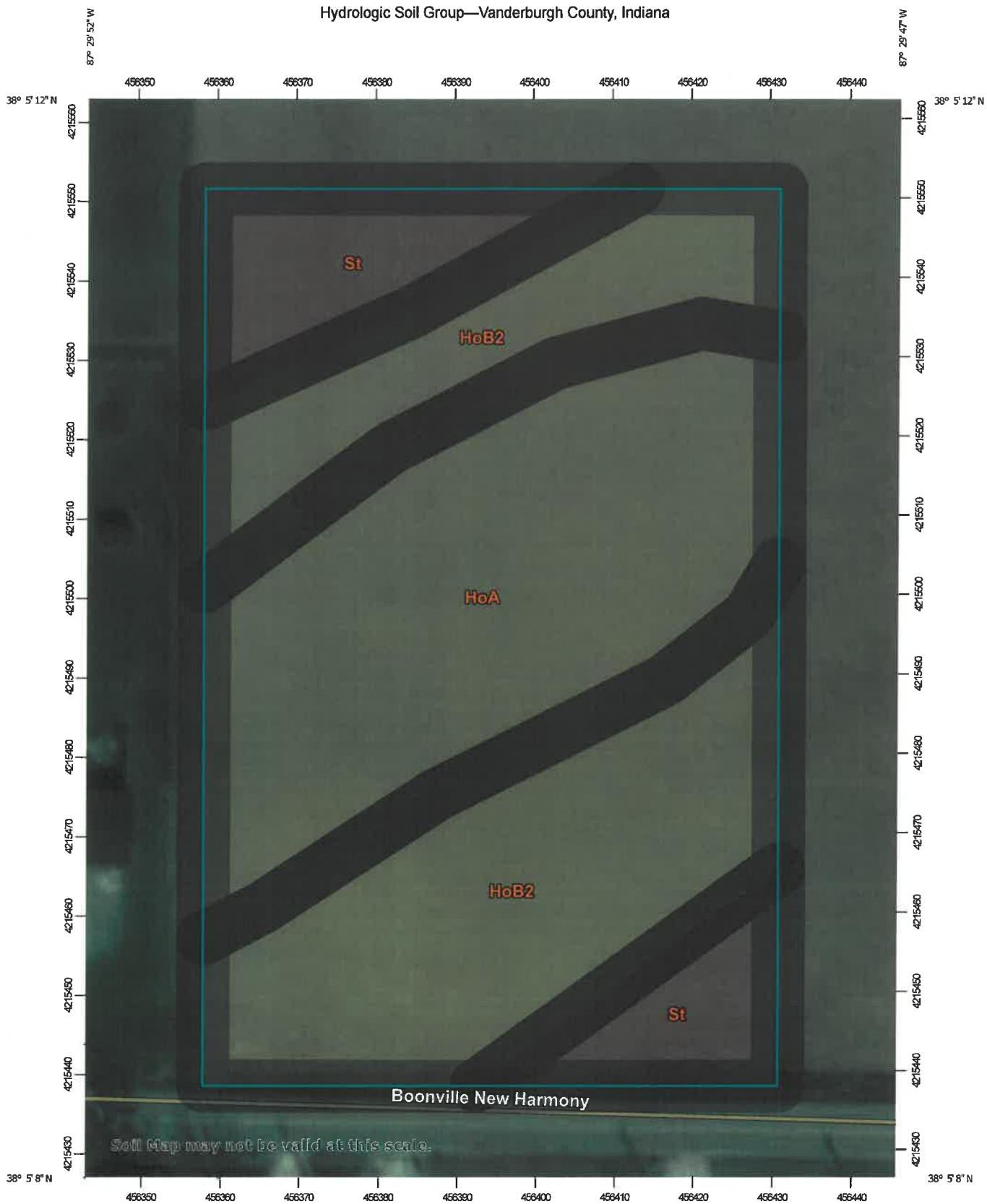
S 01°27.29" W 345.00

#### THOROUGHFARE SETBACK

N 88°56'41" W 250.00'

## **BOONVILLE - NEW HARMONY ROAD**

### Hydrologic Soil Group—Vanderburgh County, Indiana



Map Scale: 1:663 if printed on a portrait (8.5" x 11") sheet.  
Meters  
0 5 10 20 30  
Feet  
0 30 60 120 180  
Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 16N WGS84



Natural Resources  
Conservation Service

Web Soil Survey  
National Cooperative Soil Survey

1/5/2022  
Page 1 of 4

## MAP LEGEND

<b>Area of Interest (AOI)</b>		Area of Interest (AOI)		C
				C/D
<b>Soils</b>				D
		Not rated or not available		
<b>Soil Rating Polygons</b>		A		
		A/D		
		B		
		B/D		
		C		
		C/D		
		D		
		Not rated or not available		
<b>Soil Rating Lines</b>		A		
		A/D		
		B		
		B/D		
		C		
		C/D		
		D		
		Not rated or not available		
<b>Soil Rating Points</b>		A		
		A/D		
		B		
		B/D		

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:15,800.

**Warning: Soil Map may not be valid at this scale.**

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

**Source of Map:** Natural Resources Conservation Service

**Web Soil Survey URL:**

**Coordinate System:** Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS Certified data as of the version date(s) listed below.

**Soil Survey Area:** Vanderburgh County, Indiana

**Survey Area Data:** Version 21, Sep 9, 2021

**Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.**

**Date(s) aerial images were photographed:** Feb 12, 2016—Mar 9, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
HoA	Hosmer silt loam, 0 to 2 percent slopes	C/D	0.8	39.5%
HoB2	Hosmer silt loam, 2 to 5 percent slopes, eroded	C/D	0.9	44.7%
St	Stendal silt loam	B/D	0.3	15.8%
<b>Totals for Area of Interest</b>			<b>2.0</b>	<b>100.0%</b>

### Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

**Group A.** Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

**Group B.** Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

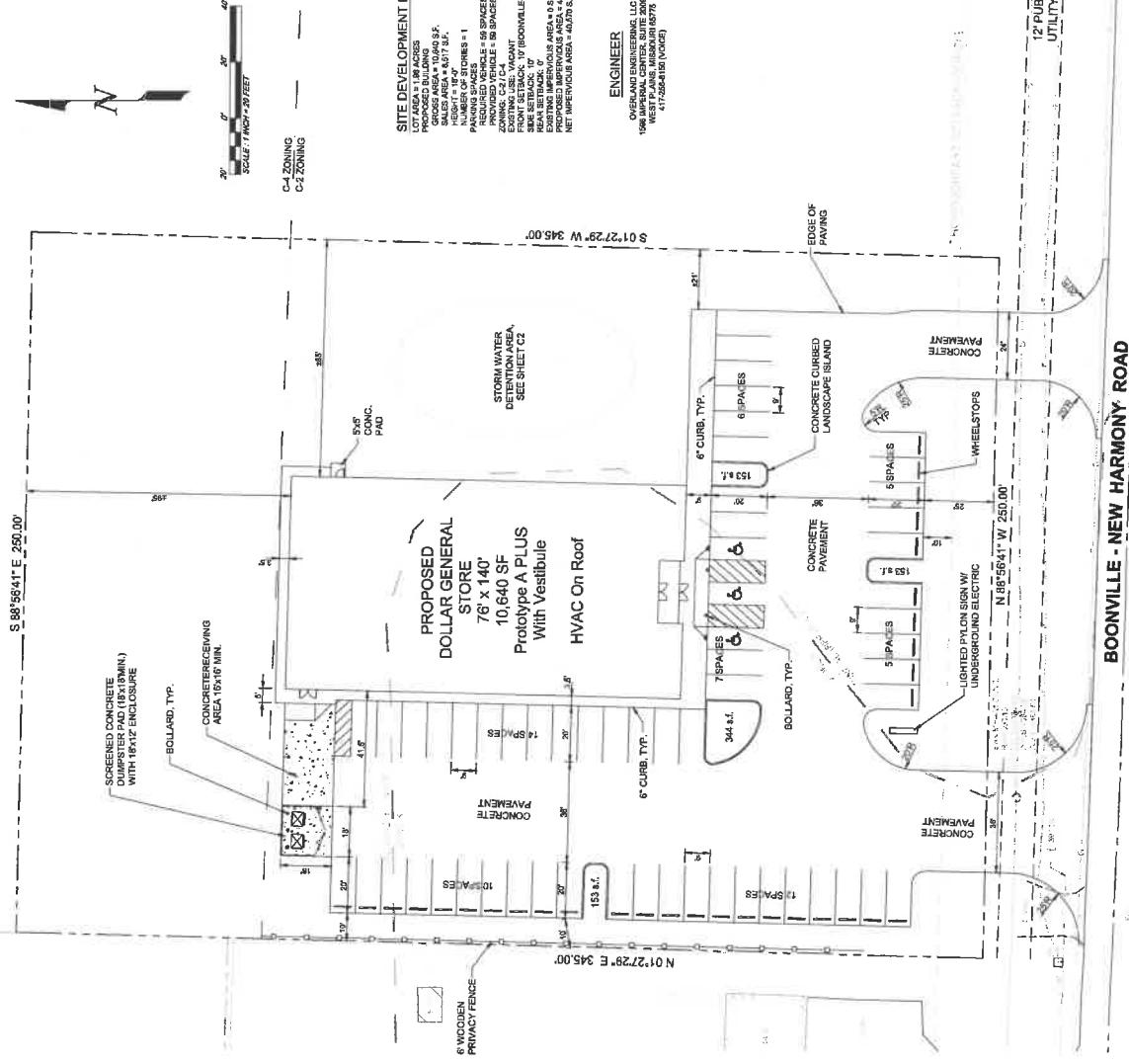
**Group C.** Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

**Group D.** Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

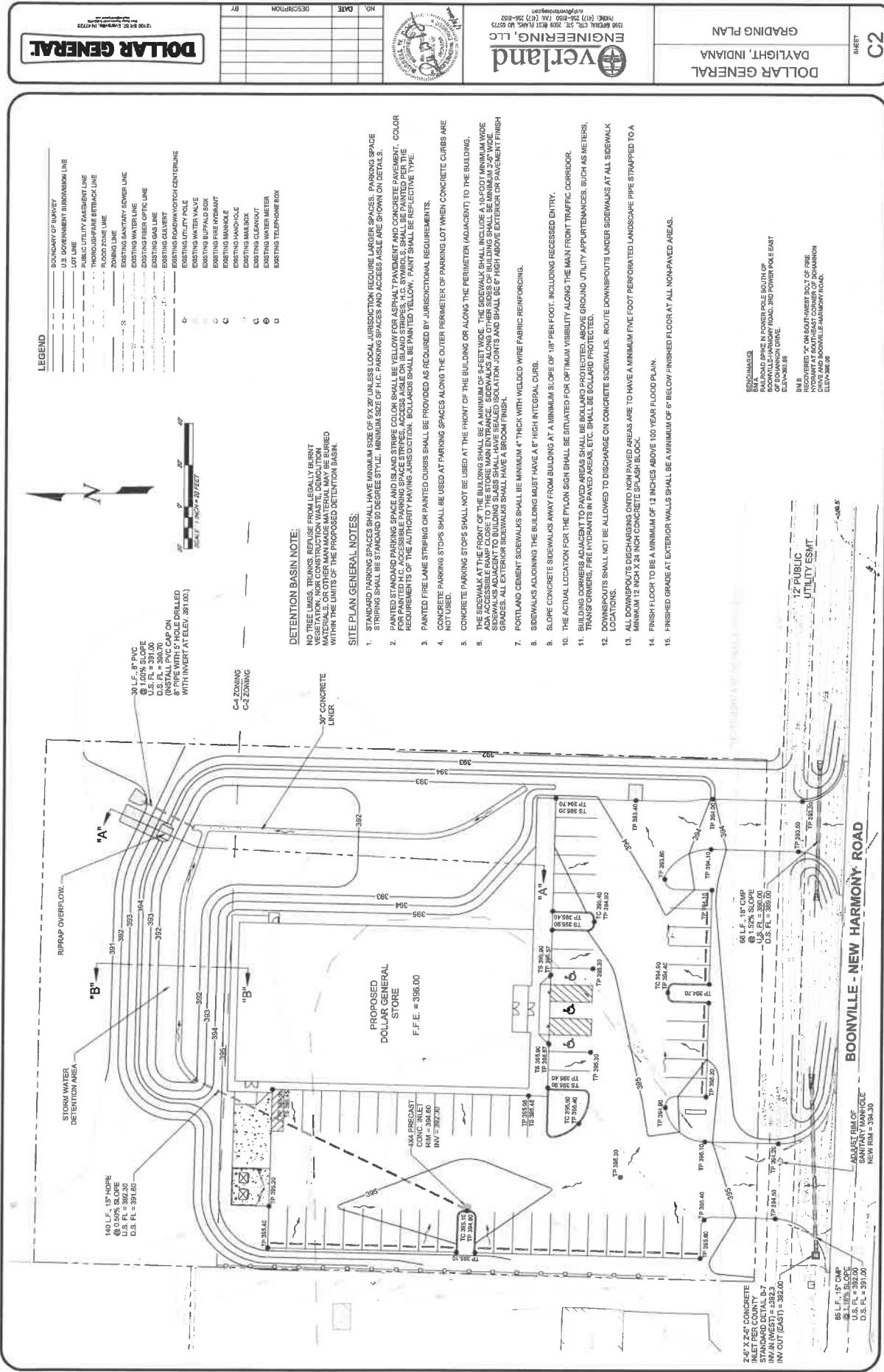
If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

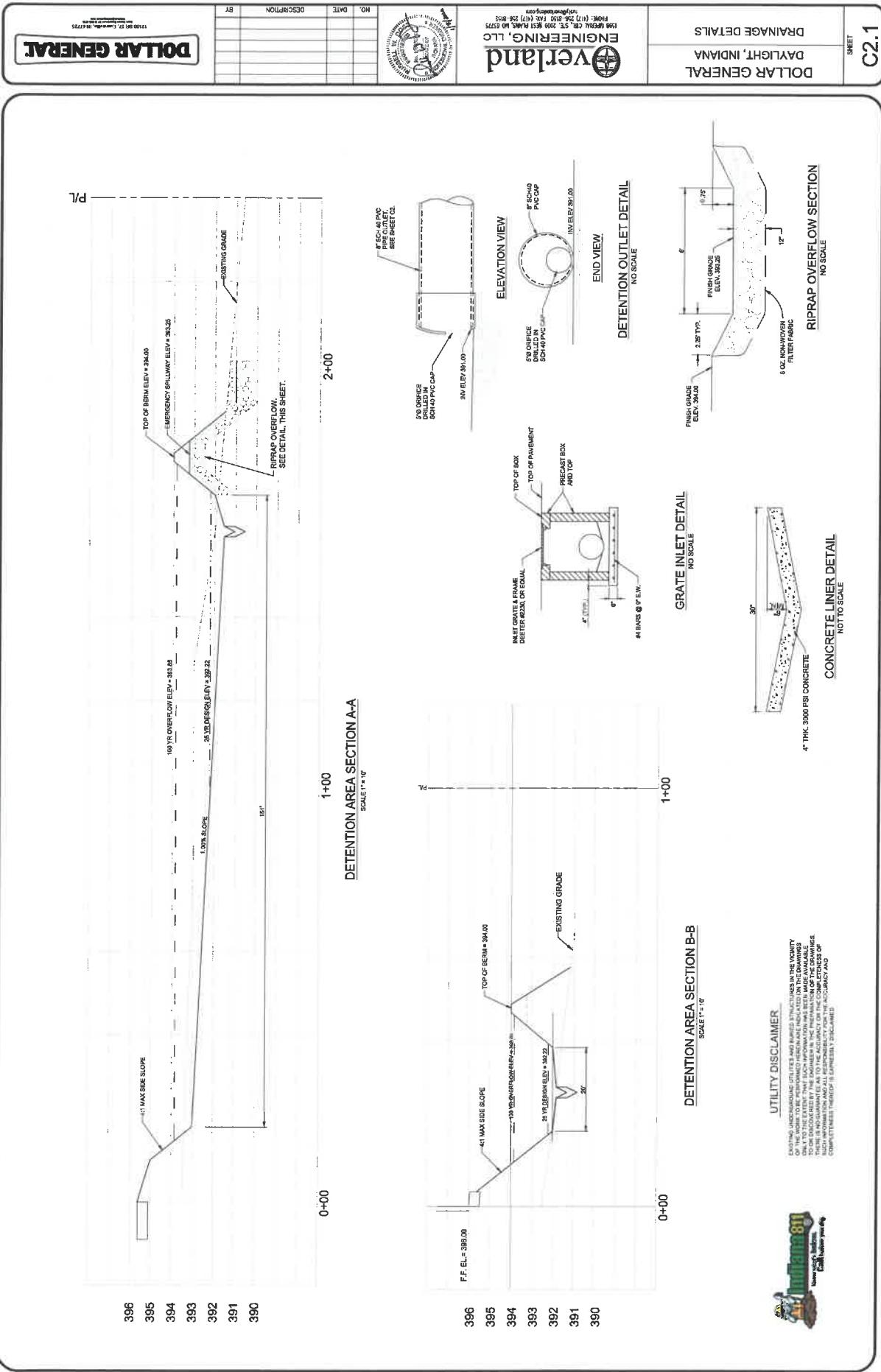


**DOLLAR GENERAL STORE**  
**DAYLIGHT, INDIANA**



DOLLAR GENERAL		NO. DATE	DESIGNATION	BY
1590 E 250 S, Suite 300, Indianapolis, IN 46222 1-800-342-8584, Fax: 317-252-9515				
<b>VErland</b> <b>ENGINEERING, LLC</b>				
SHEET <b>C1</b>				

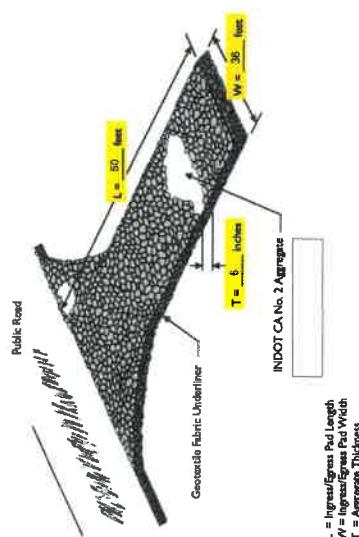






## **Concrete Washout (Above Grade System)**

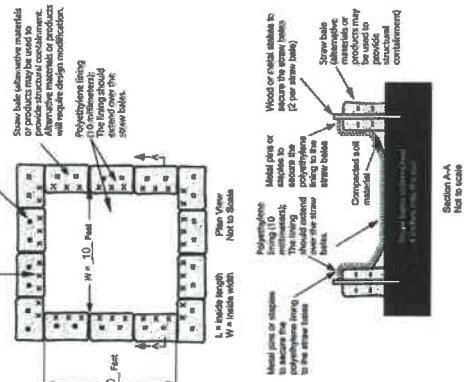
**Temporary Construction Ingress/Egress Pad  
Plan View Worksheet**  
(small sites – less than two acres)



$L$  = Ingress/Egress Pad Length  
 $W_y$  = Ingress/Egress Pad Width  
 $T$  = Antenna Thickness

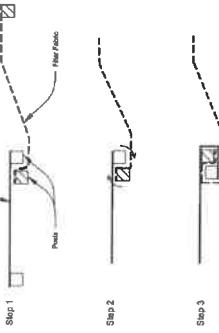
## **Concrete Washout (Above Grade System)**

Wood or metal stakes to secure the snow bank (per straw bale)



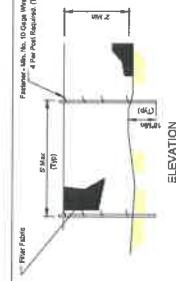
Section A-A  
N.C. 60' north

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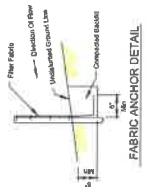


ATTACHING TWO SILT FENCES

DEFENCE PL



560



**NOTES:**

1. Temporary sediment fences will be installed prior to any grading work. They may be maintained throughout the construction period and removed in conjunction with the final grading surface stabilization.
2. Filing shall meet the requirements of insteader specification 562 (Table 1 or 2, Class 2, with equivalent opening size of at least 30 mm for nonwoven and 40 mm for woven).
3. Minimum fence height shall be 1.5 m in all areas except as noted in Table 1 or 2.
4. Minimum fence height shall be 1.8 m in areas where the potential exists for a 10-ft. high wind event.

**NOTE: EROSION CONTROL SPECIFICATIONS SHALL BE ACCORDING TO THE  
INDIANA STORM WATER QUALITY MANUAL,  
WHICH CAN BE FOUND ONLINE AT:  
<http://www.in.gov/den/stormwater/2363.htm>**

**NOTE: EROSION CONTROL SPECIFICATIONS SHALL BE ACCORDING TO THE  
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<http://www.in.gov/den/stormwater/2363.htm>**

SEEDING AND MULCHING SPECIFICATIONS

1. GOVERNING SPECIFICATIONS  
ALL SEEDING, MACHINING, FERTILIZING, AND MAINTENANCE SHALL BE IN ACCORDANCE WITH THE INDIANA DOT STANDARD SPECIFICATIONS.
2. TOPSOIL  
SEEDBED SHALL BE SMOOTH AND UNIFORM WITH PREPARED LOOSEND TOPSOIL A MINIMUM OF 3 INCHES.
3. FERTILIZER  
FERTILIZER SHALL BE 12-12-12 (N-P-K) COMMERCIAL GRADE APPLIED AT A RATE OF 200 LBS PER ACRE.
4. SEEDING  
SEED MUST BE MATURE AS SPECIFIED IN THE INDIANA DOT SPECIFICATIONS.  
SEED SHALL BE APPLIED AT A RATE OF 150 POUNDS PER ACRE.
5. MULCHING  
MULCH SHALL BE APPLIED IN A 2-INCH THICKNESS.  
MULCH SHALL BE APPLIED BY METHOD #2 OR METHOD #3 IN 24 HOURS OF FERTILIZING.
6. SEASONAL REQUIREMENTS  
SEASONAL WORK SHALL BE PERFORMED BETWEEN FEBRUARY 1 AND OCTOBER 15.

SHEET 31

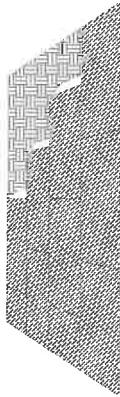
DOLLAR GENERAL



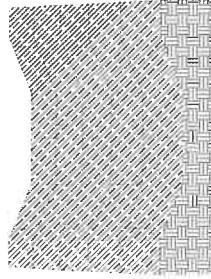
VERLAND

DOLLAR GENERAL  
DAVYLIGHT, INDIANA  
SEDIMENT & EROSION  
CONTROL DETAILS

C3.2



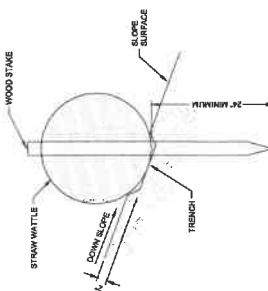
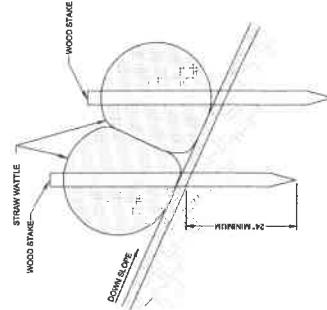
LAY SOD IN A STAGGERED PATTERN WITH STRIPS BUTTED TIGHTLY AGAINST EACH OTHER  
ON SLOPES 5' OR FEWER STAPLED TO  
FASTEN SOD FIRMLY AT THE CORNERS AND CENTERS.



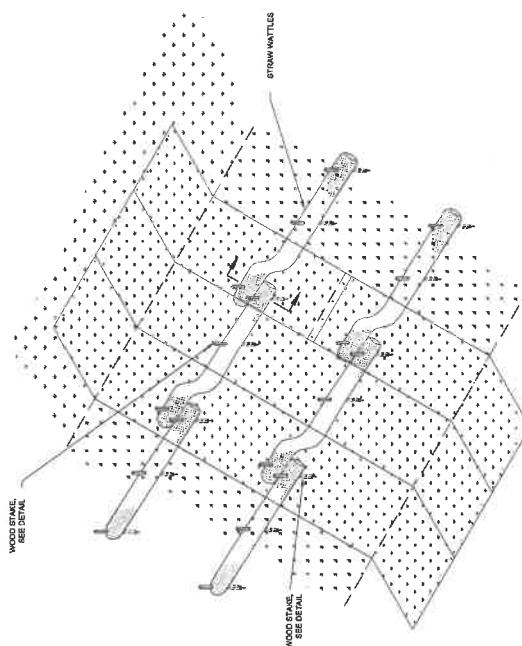
#### INSTALLATION OF GRASS SOD

LAY SOD PERPENDICULAR TO THE  
SLOPE. STAPLE SOD FIRMLY.  
SHRINKAGE IS FASTER SOD FIRMLY AT  
THE CORNERS AND CENTERS

#### INSTALLATION OF SOD IN WATERWAYS



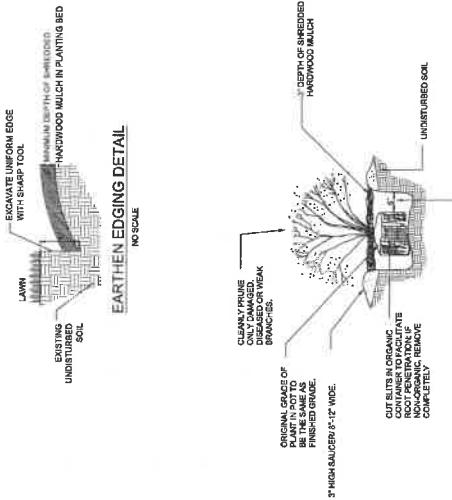
BIO-ROLLWATTLE DETAIL  
NOT TO SCALE





#### EARTHEN EDGING DETAIL

21

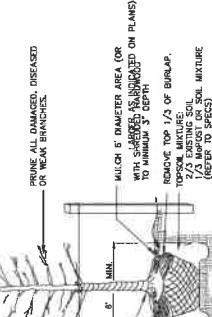


SHRUB DETAIL



104

1

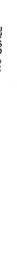


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REED DETAIL - LESS THAN 3 1/2" CALIPER

416



**DOLLAR GENERAL****VERLAND**

DOLLAR GENERAL LLC

DAYLIGHT, INDIANA

C5

TREATED PINE USE GALVANIZED NAILS FOR  
FASTENING. NO. OF PINE BOARD TO THE  
DECODED PERMIT IS FOR RESIDENTIAL USE FOR  
RESIDENTIAL USE OR IS ACTUALLY BEING USED FOR  
RESIDENTIAL USE IN CONSIDERATION OF RESIDENTIAL PROPERTY).

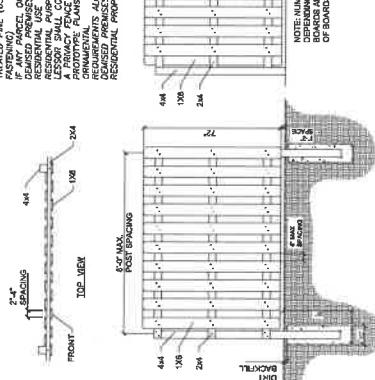
A PRIMARY FENCE IN ACCORDANCE WITH TENANT'S

REQUIREMENTS ALONG ANY PORTION OF THE

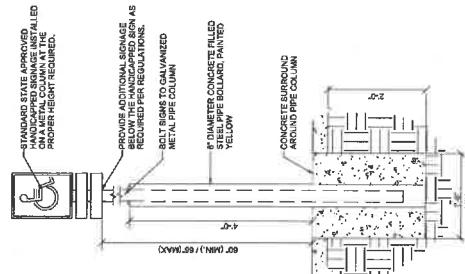
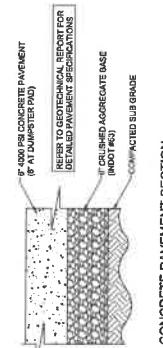
CODED PERMIT BOUNDING UPON SUCH

RESIDENTIAL PROPERTY.

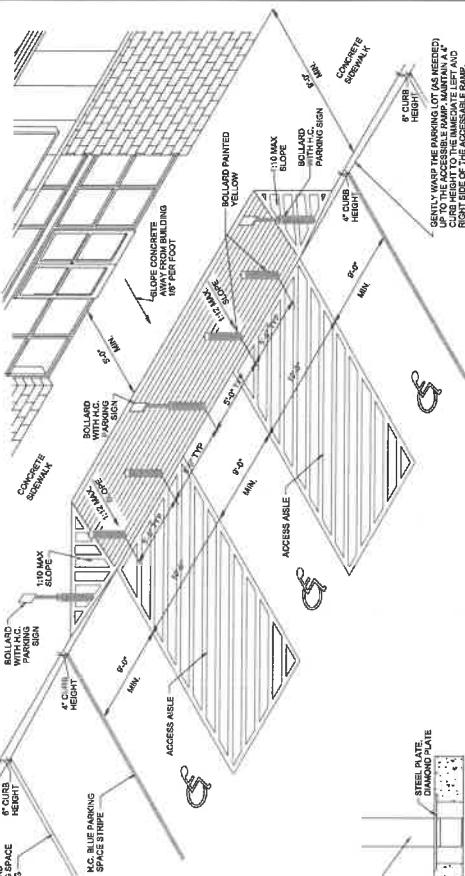
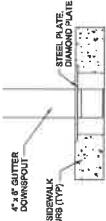
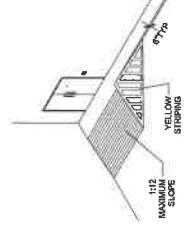
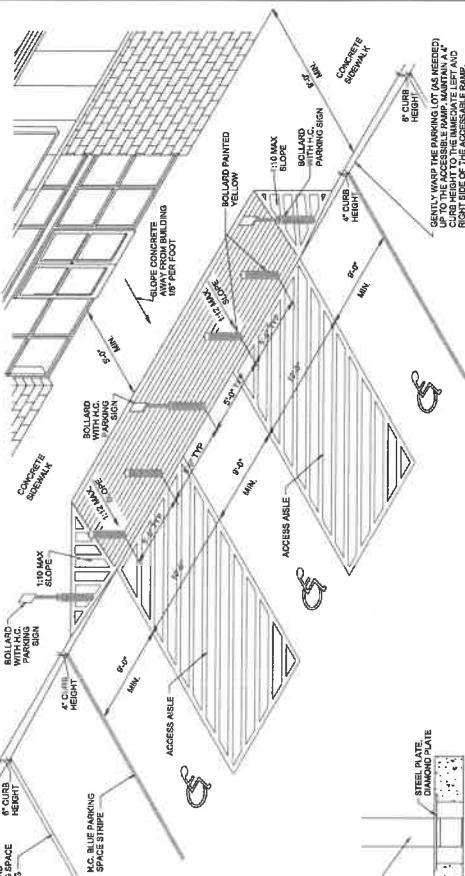
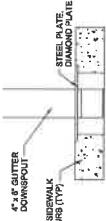
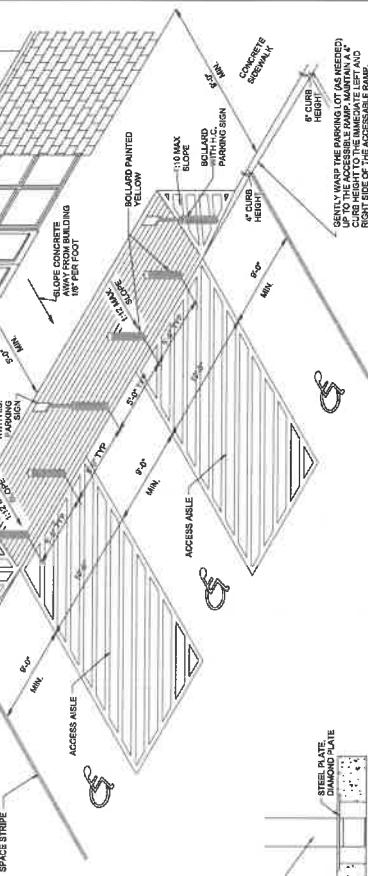
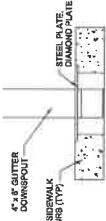
NOTE: NUMBER OF BOARDS WILL VARY  
DEPENDING ON SPACE BETWEEN  
BOARD AND ACTUAL WIDTH  
OF BOARD.



FRONT VIEW

**WOOD FENCE DETAIL**  
NOT TO SCALE

**BOLLARD DETAIL**  
NOT TO SCALE

**CONCRETE PAVEMENT SECTION**  
NOT TO SCALE

**STRIPPING NOTES**  
YELLOW CURBING  
AND BOLLARDS  
SURFACES SHOULD BE CLEAN, DRY AND METAL SURFACES  
FREE OF HEAVY RUST 2 COATS SHEWWIN WILLIAMS - KEM-4000  
ACRYLIC ALKYL ENAMEL SAFETY YELLOW 1957300  
SHEWIN WILLIAMS - FROMAR TRAFFIC MARKING  
PAINT YELLOW TMS95  
HANDICAP  
SPACING  
PARKING LOT  
SURFACES SHOULD BE CLEAN, DRY, TOP COAT  
PAINT 1/2 C. THICKNESS - FROMAR TRAFFIC MARKING  
PAINT TMS95

**FRONT ENTRY ISOMETRIC**  
NOT TO SCALE**GUTTER DOWNSPOUT DETAIL**  
NOT TO SCALE**SIDE ENTRY DETAIL**  
NOT TO SCALE**FRONT ENTRY ISOMETRIC**  
NOT TO SCALE**GUTTER DOWNSPOUT DETAIL**  
NOT TO SCALE**FRONT ENTRY ISOMETRIC**  
NOT TO SCALE**GUTTER DOWNSPOUT DETAIL**  
NOT TO SCALE

*Supplement 2/15/22*

DOLLAR GENERAL #24125  
HYDRAULIC CALCS  
BY: Overland Engineering LLC  
Date: 2/15/2022

Rational Method, Q = CIA

Pre Project

TR 55 Method

Sheet Flow

Flow length 100 ft  
Land slope 0.01 ft/ft  
Manning's n 0.15 Short Grass  
2 yr/24hr rainfall 3.3 in

t = 12.7 min

Shallow concentrated flow

Flow length 175 ft  
Slope 0.017 ft/ft  
Avg. velocity 2.10 ft/s

Unpaved t = 1.4 min

Open channel flow

Flow length 0 ft  
Avg. velocity 2.0 ft/s

t = 0.0 min

Tc = 14.1

Post Project

TR 55 Method

Sheet Flow

Flow length 40 ft  
Land slope 0.01 ft/ft  
Manning's n 0.011 Pavement  
2 yr/24hr rainfall 3.3 in

t = 0.8 min

Shallow concentrated flow

Flow length 150 ft  
Slope 0.01 ft/ft  
Avg. velocity 2.03 ft/s

PAVED t = 1.2 min

Open channel flow

Flow length 240 ft  
Avg. velocity 2.0 ft/s

t = 2.0 min

Tc = 4.0

Tc (total) = 14.00 min

Tc (total) = 5.00 min (use 5 minute min.)

Intensity z= 3.51 in/hr

Intensity 10= 4.65 in/hr

Weighted Runoff C

c <sub>1</sub> =	0.94	Paved Areas
A <sub>1</sub> =	0.00	
c <sub>2</sub> =	0.12	Grass/Lawns
A <sub>2</sub> =	1.34	

Drain Area Total = 1.34 acres

C (composite) = 0.12

Q<sub>2</sub> = 0.56 cfs

Q<sub>10</sub> = 0.75 cfs

Intensity z= 5.02 in/hr

Intensity 10= 6.66 in/hr

Intensity 25= 7.81 in/hr

Intensity 50= 8.82 in/hr

Intensity 100= 9.95 in/hr

Weighted Runoff C

c <sub>1</sub> =	0.92	Paved Areas
A <sub>1</sub> =	0.93	
c <sub>2</sub> =	0.15	Open Spaces
A <sub>2</sub> =	0.41	

Area Total = 1.34 acres

C (composite) = 0.68

Q<sub>2</sub> = 4.57 cfs

Q<sub>10</sub> = 6.07 cfs

Q<sub>25</sub> = 7.12 cfs

Q<sub>50</sub> = 8.04 cfs

Q<sub>100</sub> = 9.07 cfs

25 year - Using Q<sub>10</sub><sub>pre</sub> as allowable outflow

Rainfall Duration (min)	25 yr Rainfall Intensity (in/hr)	Inflow Rate (in-acre/hr)	Allowable Max Outflow (cfs)	Required Storage	Det Volume (acre-ft)	Det Volume (ft <sup>3</sup> )
0	—	—	—	—	—	—
5.00	7.81	7.12	0.75	6.37	0.04	1,927
6.00	7.51	6.84	0.75	6.10	0.05	2,213
7.00	7.21	6.57	0.75	5.82	0.06	2,466
8.00	6.91	6.30	0.75	5.55	0.06	2,686
9.00	6.61	6.02	0.75	5.28	0.07	2,872
10.00	6.32	5.76	0.75	5.01	0.07	3,032
11.00	6.10	5.56	0.75	4.81	0.07	3,201
12.00	5.88	5.36	0.75	4.61	0.08	3,347
13.00	5.66	5.16	0.75	4.41	0.08	3,468
14.00	5.44	4.96	0.75	4.21	0.08	3,565
15.00	5.24	4.77	0.75	4.03	0.08	3,654
17.50	4.92	4.48	0.75	3.74	0.09	3,955
20.00	4.60	4.19	0.75	3.44	0.10	4,167
25.00	3.80	3.46	0.75	2.71	0.09	4,106
30.00	3.31	3.02	0.75	2.27	0.09	4,117
40.00	2.58	2.35	0.75	1.60	0.09	3,880
45.00	2.31	2.10	0.75	1.36	0.08	3,695
50.00	2.08	1.90	0.75	1.15	0.08	3,471
60.00	1.95	1.78	0.75	1.03	0.09	3,736
90.00	1.67	1.52	0.75	0.77	0.10	4,214
120.00	1.37	1.25	0.75	0.50	0.08	3,635
180.00	1.02	0.93	0.75	0.18	0.05	1,979
240.00	0.82	0.75	0.75	0.00	0.00	-8

Detention Vol Reqd = Maximum = 4,214

### **Detention Volume Provided**

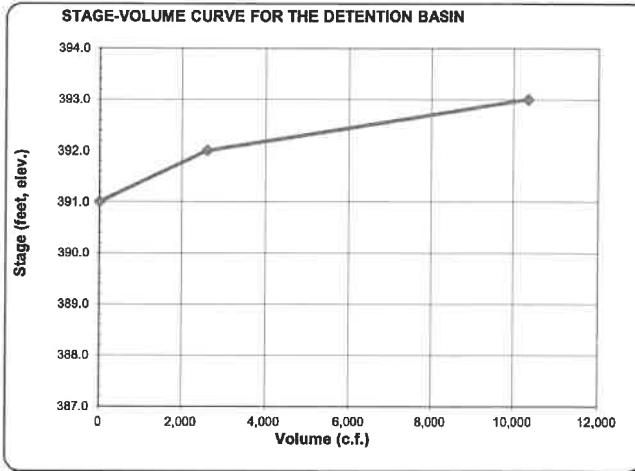
CONIC VOLUME				
Water Surface Elevation ft (input)	Corresponding Contour Area square feet (input)	Volume above Datum acre-ft (output)	Volume above Datum Cubic Feet (output)	
391.0	0	0.000	0	
392.0	5,194	0.060	2,597	
393.0	10,306	0.238	10,347	

#### Required Storage Elevation with 10% Additional for Sedimentation

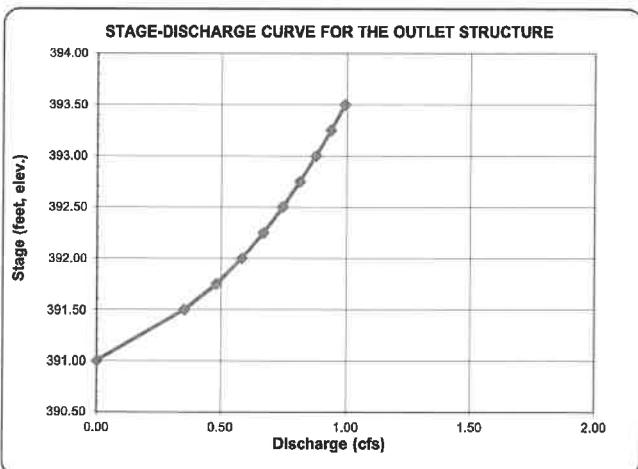
ELEV<sub>10</sub> = 392.27 ft Total Volume = 4690 c.f.

## Outlet Structure Design

Outlet Structure Design Inputs		Low Flow	Weir 1
5" Orifice @ 391.21	cfs		
391.00	0.00	L =	6.00
391.50	0.35	C <sub>w</sub> =	2.70
391.75	0.48	E <sub>o</sub> =	393.50
392.00	0.58	Manning's n-values	
392.25	0.67	PVC	0.012
392.50	0.74	PE (<9"dia)	0.015
392.75	0.81	PE (>9"dia)	0.02
393.00	0.88	PE(9-12"dia)	0.017
393.25	0.94	CMP	0.024
393.50	0.99	ADS N12	0.012
		Cenc	0.013



### Rating Curve of Outlet Structure



### **Compare Outflow Elevation to Required Storage Elevation**

Max Outflow cfs	Occurs at Elevation	Required Elevation	At or above req.?
Q <sub>10 allowable</sub> = 0.75	392.51	392.27	YES

**Detention Basin Maintenance Plan**  
**Dollar General**  
**12100 SR57**

The detention basin proposed for the southern portion of the project site includes 4,758 c.f. of storage volume, a concrete liner, a pvc pipe outlet, and a riprap emergency overflow spillway. The concrete liner is intended to provide positive drainage to the pvc pipe outlet, minimizing wet areas in the bottom of the basin. The pvc outlet pipe is the primary control and will function to drain the basin during normal rainfall events. The riprap overflow spillway will function only during major storm events when the capacity of the pvc outlet pipe is unable to convey the peak runoff.

Routine maintenance of the detention basin shall include:

**Inspections:** Monthly inspections and inspections after major rainfall events to check for obstructions/damage & to remove debris/ trash.

**Vegetation Management:** Mowing on a regular basis to prevent erosion and aesthetic problems. Collect grass clippings and all other clippings/trimmings and take offsite for disposal or dispose in trash on site; do not leave in the pond. Remove vegetation adjacent to outlet works that may interfere with operation; note if noxious weeds present and schedule treatment/removal. Limit use of fertilizers and pesticides in and around the ponds to minimize entry into pond and subsequent downstream waters.

**Trash, debris and litter removal:** Removal of any trash, etc causing any obstructions at the inlet or outlet during and especially after every runoff producing rainfall event. General pickup of trash, etc in and around the pond during all inspections.

**Structural Component check:** Inspection of the inlet and outlet on a regular basis for additions to the annual Non-routine Maintenance list

Non-routine maintenance shall include:

**Bank erosion/stabilization:** It is critical to keep effective ground cover on all vegetated areas in order to see the benefits of proper infiltration of runoff, and effective filtering of pollutants. All areas not vegetated should be re-vegetated and stabilized immediately

**Sediment removal:** Every six months or so, the accumulated sediment should be removed from the bottom of the basin. When the depth of the accumulated sediment is 10% (330 c.f.) of the original design volume, sediment should be removed.

**Structural Repair/Replacement:** Repair or replacement of the inlet and outlet as necessary.