

***FINAL***  
**STORM DRAINAGE ANALYSIS**

**CASTLE CREEK SUBDIVISION**  
Highway 41 North at Schroeder Road  
Evansville, Indiana

*BLA Project No. 197-0181-APD*


*Prepared for:*

Castle Properties, Inc.  
2626 Kotter Avenue  
Evansville, IN 47715

*By:*

Bernardin • Lochmueller & Associates, Inc.  
6200 Vogel Road  
Evansville, Indiana 47715  
812-479-7200

January 8, 2001

Rec'd 1-11-001  


## INTRODUCTION

The proposed Castle Creek Subdivision is to be constructed along the Highway 41 North corridor at the northeast quadrant of the intersection of Schroeder Road and U.S. Highway 41 North in Evansville, Indiana. A part of this site falls within the 100 year Zone "A", as noted on Community Panel No. 180256 0015 C of the Flood Insurance Rate Maps dated August 5, 1991. A complete hydraulic study has been undertaken to determine the 100 year flows and floodway for the adjoining Rusher Creek that flows east to west along the north side of this development. The proposed commercial/light industrial park is situated on cultivated fields ranging in slope from 2% to 5%. The soils are predominantly silt loams. The entire tract drains from east to west and from south to north toward Rusher Creek. In June of 2000 a preliminary drainage plan showing a large pond constructed on Lot 7 was presented to the Drainage Board and approved.

In the interim, after consulting with marketing consultants, the Owner has requested that a very linear storm retention facility be designed stretching across many of the lots in lieu of the plan originally approved. Contained in this report is a revised report which will address the storm detention requirements for this proposed development in accordance with the current Vanderburgh County Drainage Ordinance. This ordinance states that a 10 year undeveloped condition should be compared to a ~~25~~ year developed condition and the quantitative difference in runoff experienced under these conditions be temporarily detained. Due to the sensitivity of drainage throughout this area, the county has deemed this an impacted area and therefore the 100 year developed conditions will be compared to the 10 year undeveloped condition.

There are 27 acres (plus or minus) east of this project that drains through the subject property by way of a 36 inch diameter pipe beneath that section of Schroeder Road that runs north/south and lies east of the subject property. There is also approximately seven acres south of this project that drains through this site by way of an 18 inch diameter pipe beneath that section of Schroeder Road that runs east/west and lies to the south of the subject property.

These offsite flows will be routed through the basin rather than around the site because, due to the very flat terrain and lay of the land, routing the offsite stormwater completely around the site will be very difficult. The offsite flows will enter the long linear drainage basin at Schroeder Road to the east and also Schroeder Road to the south. The stretch of ditch from Schroeder Road east to Castle Creek Drive will remain a dry drainage-way and, due to the very flat, longitudinal grade, the invert will be paved. ✓

A wet facility is proposed for that length of ditch north from Schroeder Road (south) to Rusher Creek Road (west) and then west from this juncture to the Highway 41 right-of-way, then again from this juncture north along Highway 41 to the northwest corner of the project. 1250  
INDOT  
?

This rather long, lineal drainage basin will provide storm detention for nearly all of the runoff from within the site. A dual stage outlet structure will be installed at the northwest corner of the basin which will help throttle the smaller storms while also providing the overflow capacity necessary for the larger storms where much offsite runoff must route through the basin. ✓

## METHOD

The rational Method ( $Q = cia$ ) will be used to compute the 1 and 10 year undeveloped flows. This flow rate will be determined by analyzing the entire watershed area since it will be routed through the basin. The summation of this flow, inclusive of the offsite area that drain through this site, will be used as the allowable outflow rates for the developed site.

"c" = Runoff Coefficient. The existing land slopes from west to east. The soils are silt loams. The area is currently cultivated fields ranging from 2% to 5% in slope. Table 3.2.1 of the drainage ordinance suggests an undeveloped runoff

coefficient of 0.50 be used. This value will be used to determine both onsite and offsite flows.

"i" = Intensity. Kerby's Formula will be used to determine the Time of Concentration for the undeveloped site and the corresponding 10-year intensity will be calculated. For the area flowing from the south and east towards the basin, a value of 66 minutes was calculated. The resulting 10-year intensity equals 1.33 (see Appendix "B").

"a" - Area. The entire contributory area flowing into the basin from the proposed site and the associated offsite areas is approximately 74 acres (less INDOT right-of-way).

In addition, a developed "c" factor of 0.7 will be used on the proposed land use and anticipated surface improvements.

To the product of the developed "c" value and the area "a", a range of intensity values for different duration storms having a 25 year and 100 year specified returns rate will be multiplied to compute expected inflow rates from the subdivision.

The difference between the inflow rates and outflow rates for each interval will establish the required storage for that interval. From this data a curve can be generated and the peak or largest value attained will be used as the required storage basin capacity.

This conventional method of determining the allowable outflow is the most utilized method of analyzing the site as outlined in the drainage ordinance, however, due to the very linear nature of the basin (which is actually a series of basins having pool elevations of 444, 446 and 447) this site cannot be analyzed adequately with the approach outlined above. Designing a series of basins set one behind the other and installing walls with weir outlet configurations built into them between the lakes will



allow for much storage in the basins. Although the allowable outflow computed using the Rational Formula, as described herein, will be the maximum design outflow, the nature of the basins set in series will result in a final outflow from the northern-most basin being significantly less than the allowable 45 CFS. ✓

Each weir set to control pool elevations will in itself act to limit the discharge of stormwater as it moves through the linear drainage basin. Each basin will be designed to fill to capacity. The stormwater release from the last lake in the series will be controlled through a dual stage outlet structure and outlet pipe sized to keep the release rate well below the allowable outflow.

## RESULTS

The allowable 10 year outflow rate for the developed site is 45 CFS. This value was calculated using the Rational Method (see appendix C).

Using a sophisticated modeling program, the site was modeled as a series of lakes working together to detain the runoff and a summary of the calculation results of the computer run are as follows:

BASIN	PEAK FLOW (CFS)	MAX. POND STORAGE (Acre/Feet)	MAXIMUM WATER SURFACE ELEVATION (Feet)
A	4.23	0.214	448.90
B	4.50	0.218	448.63
C	21.67	0.507	448.39
D	31.57	1.52	448.06
E	31.97	0.272	447.40
F	3.43	0.422	446.31
G	37.11	1.406	446.33

Maximum outflow leaving site (Basin G) = 37.11 CFS

Total Available Storage needed per analysis (Summation Basins A thru G) = 4.559 acre feet

There is a total of 6.65 acre/feet of storage available in the basins. The total storage needed per this analysis is 4.559 acre feet. This exceeds the 3.42 required by requirements set forth in the Vanderburgh County Drainage Ordinance for the 100 year storm (See Appendix C).

By utilizing a complex software package we have controlled the outflows and reduced the final outflow to a value of 37.1 CFS, which is also less than the 45 CFS allowed by ordinance (refer to calculations in Appendix C). This outflow was modeled with a tailwater of the final outlet pipe being influenced by the headwater of Rusher Creek.

### **SUMMARY**

An association of lot owners will assume maintenance of the proposed storm water facility.

All runoff from all paved area and rooftops constructed on all of the lots and the two adjoining areas to the east and south of this project will be routed through this basin. In addition, the runoff from the public roadways within the dedicated site will be routed through this basin.

The roadside ditch along Schroeder Road south and east of the project will also be routed through the basin.

All stormwater modeling 10/100 exceeds the requirements set by INDOT for projects adjacent to INDOT facilities.

By utilizing Pond Pack and capitalizing on the available stormwater storage capacity in these ponds, we can control the release rate to much less than that required as previously stated in the results.

Minimum building elevations on all lots on this site should be set by the Building Commissioner in accordance with both the results of this report and the hydraulic study for Rusher Creek performed independently of this report. With this linear stormwater retention facility, the maximum 100 year ponding elevations vary from basin to basin.

We believe that with this report and the independently performed 100 year Floodway Analysis for Rusher Creek a very good database has been provided. This data base should serve as a guidance tool for the best and safest utilization of this property.

OK PER CO. SURVEYOR  
w/:

1. Floodway Approval DNR
2. IDOT Approval discharge into  
R/W if needed
3. Commission approval of  
any detention/conveyance  
open Basins/waterways  
in Dedicated R/W

## APPENDICES INDEX

- Appendix A - Drainage Plan
- Appendix B - Time of Concentration / Intensity
- Appendix C - Storage Volume Data
- Appendix D - Outlet Control Structure (utilizing Culvert software)
- Appendix E - Basin Volumes
- Appendix F - Stormwater Analysis (utilizing Pond Pack software)

see separate Table of Contents for summary of:

- A. Design Storm
  - B. Pond Volumes
  - C. Outlet Structure
  - D. Pond Routing
-



**APPENDIX "A"**  
**DRAINAGE PLAN**

---

**APPENDIX "B"**

**TIME OF CONCENTRATION / INTENSITY**

---

## TIME OF CONCENTRATION

### SHEET FLOW

$$TC = .827 \left[ \frac{(N)(L)}{\sqrt{S}} \right]^{.467}$$

N = 0.4 Coefficient Grass

L = Length

S = Slope

L = 3000'

H = 580 - 550 = 30 feet

S = .01

$$TC = .827 \left[ \frac{(0.4)(3000)}{\sqrt{S}} \right]^{.467} = 66 \text{ minutes}$$

### INTENSITY

$$i = \frac{C(T)^\alpha}{(Tc+d)^\beta}$$

#### Factors for Evansville

C = 1.9533

T = duration

$\alpha$  = 0.1747

Tc = Time of Concentration (10 yr. undeveloped)

d = 0.522

$\beta$  = 1.6408

$$i_{10} = \frac{1.9533(10)^{0.1747}}{(66/60+0.522)^{1.6408}} = \frac{2.9361}{2.211} = 1.33$$

**APPENDIX "C"**

**STORAGE VOLUME DATA**

---

Sub daily

PROJECT: CASTLECRE  
ENGINEER:

DATE: \*\*\*\*\*

RELEASE RATE PERIOD: 5\10\25\100  
WATERSHED AREA (ACRES): 40  
TIME OF CONCENTRATION UNDEV. (min): 39  
RAINFALL INTENSITY (INCHES/HR): 2.70 2.250985 2.302636

UNDEVELOPED RUNOFF COEFFICIENT: 0.5  
UNDEVELOPED RUNOFF RATE (CFS): 45.02  
DEVELOPED RUNOFF COEFFICIENT: 0.7

25 YEAR STORM

STORM DURATION (HRS)	RAINFALL INTENSITY (INCH/HR)	INFLOW RATE (CFS)	OUTFLOW RATE (CFS)	STORAGE RATE (CFS)	REQUIRED STORAGE (ACRE-FT)	
0.08	8.02	224.44	45.02	179.42	1.196	6.85
0.17	6.20	173.54	45.02	128.53	1.821	5.45
0.25	5.26	147.41	45.02	102.39	2.133	4.65
0.33	4.62	129.34	45.02	84.32	2.319	4.15
0.42	4.09	114.42	45.02	69.40	2.429	3.80
0.50	3.72	104.17	45.02	59.15	2.465	3.40
0.58	3.42	95.84	45.02	50.82	2.457	3.20
0.67	3.15	88.12	45.02	43.10	2.406	2.85
0.75	2.94	82.34	45.02	37.32	2.333	2.75
0.83	2.76	77.36	45.02	32.34	2.237	2.60
0.92	2.59	72.49	45.02	27.47	2.106	2.45
1.00	2.45	68.70	46.05	22.64	1.887	2.30
1.25	2.11	59.20	46.05	13.15	1.370	2.05
1.50	1.86	52.15	46.05	6.09	0.762	1.85
1.75	1.67	46.67	46.05	0.62	0.090	1.60
2.00	1.51	42.27	46.05	-3.78	-0.630	1.40
2.50	1.27	35.63	46.05	-10.43	-2.172	1.25
3.00	1.10	30.82	46.05	-15.24	-3.809	1.10
4.00	0.87	24.27	46.05	-21.78	-7.259	0.84

PEAK STORAGE (ACRE/FT): 2.46  
PEAK STORAGE (CUBIC FT): \*\*\*\*\*



100 YEAR STORM

STORM DURATION (HRS)	RAINFALL INTENSITY (INCH/HR)	INFLOW RATE (CFS)	OUTFLOW RATE (CFS)	STORAGE RATE (CFS)	REQUIRED STORAGE (ACRE-FT)
0.08	9.52	266.63	45.02	221.61	1.477
0.17	7.40	207.09	45.02	162.07	2.296
0.25	6.30	176.38	45.02	131.36	2.737
0.33	5.54	155.10	45.02	110.08	3.027
0.42	4.91	137.48	45.02	92.46	3.236
0.50	4.48	125.35	45.02	80.33	3.347
0.58	4.12	115.48	45.02	70.46	3.406
0.67	3.80	106.32	45.02	61.30	3.422
0.75	3.55	99.45	45.02	54.43	3.402
0.83	3.34	93.52	45.02	48.50	3.355
0.92	3.13	87.73	45.02	42.71	3.274

1.00	2.97	83.21	46.05	37.15	3.096
1.25	2.57	71.87	46.05	25.82	2.690
1.50	2.27	63.43	46.05	17.38	2.173
1.75	2.03	56.87	46.05	10.81	1.577
2.00	1.84	51.59	46.05	5.54	0.923
2.50	1.56	43.59	46.05	-2.46	-0.512
3.00	1.35	37.79	46.05	-8.26	-2.065
4.00	1.07	29.88	46.05	-16.18	-5.392
			46.05		

PEAK STORAGE (ACRE/FT) : 3.42  
 PEAK STORAGE (CUBIC FT) : \*\*\*\*\*

**APPENDIX "D"**

**OUTLET CONTROL STRUCTURE**

---

## OUTLET CONTROL STRUCTURE

### Primary Outlet Pipe or Opening in Face of Outlet Structure

$$Q = cdA \sqrt{2gh}$$

$$cd = C_c \times C_v = (.62)(.97) = .60$$

Allow Outflow  $Q = 45$  cfs

Allow HW = Top Box Outlet Str. To IE Lower-Water Outlet Pipe

$$(45) = Q = (.60)(A) \sqrt{2(32.2)(3.75)}$$

$$A = \frac{45}{9.32} = 0.333 = \frac{\Pi d^2}{4}$$

$$d = 2.50 = 30" \text{ diameter hole in box or } 16" \times 42" \text{ rectangular opening}$$

See HY8 Computer Runs which follow

### Secondary Outlet Pipe

30" round or 16"x42" rectangular opening with 3.75' of head will pass 45 cfs and 42" diameter outlet pipe with 9' of head working against a 7' tail water will pass 8.5 cfs. 1 Twin "E" casting in top box with 42" outlet pipe will provide secondary outlet should lake fill up to within 1' of top of dam

---

CURRENT DATE: 01-08-2001  
 CURRENT TIME: 16:30:03

FILE DATE: 01-08-2001  
 FILE NAME: CAS

FHWA CULVERT ANALYSIS  
 HY-8, VERSION 6.0

C U L V E R T N O.	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (ft)	OUTLET ELEV. (ft)	CULVERT LENGTH (ft)	BARRELS SHAPE MATERIAL	SPAN (ft)	RISE (ft)	MANNING n	INLET TYPE
1	438.00	437.90	46.00	1 RCP	2.50	2.50	.012	CONVENTIONAL
2								
3								
4								
5								
6								

SUMMARY OF CULVERT FLOWS (cfs)

FILE: CAS

DATE: 01-08-2001

ELEV (ft)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
446.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
446.04	6.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
446.17	12.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
446.39	18.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
446.69	24.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
447.08	30.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
447.55	36.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
448.11	42.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
448.43	45.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
449.49	54.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
450.31	60.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0
0.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	OVERTOPPING

SUMMARY OF ITERATIVE SOLUTION ERRORS

FILE: CAS

DATE: 01-08-2001

HEAD ELEV (ft)	HEAD ERROR (ft)	TOTAL FLOW (cfs)	FLOW ERROR (cfs)	% FLOW ERROR
446.00	0.000	0.00	0.00	0.00
446.04	0.000	6.00	0.00	0.00
446.17	0.000	12.00	0.00	0.00
446.39	0.000	18.00	0.00	0.00
446.69	0.000	24.00	0.00	0.00
447.08	0.000	30.00	0.00	0.00
447.55	0.000	36.00	0.00	0.00
448.11	0.000	42.00	0.00	0.00
448.43	0.000	45.00	0.00	0.00
449.49	0.000	54.00	0.00	0.00
450.31	0.000	60.00	0.00	0.00

<1> TOLERANCE (ft) = 0.010

<2> TOLERANCE (%) = 1.000

CURRENT DATE: 01-08-2001  
 CURRENT TIME: 16:30:03

FILE DATE: 01-08-2001  
 FILE NAME: CAS

PERFORMANCE CURVE FOR CULVERT 1 - 1( 2.50 (ft) BY 2.50 (ft)) RCP

DIS- CHARGE FLOW (cfs)	HEAD- WATER ELEV. (ft)	INLET CONTROL DEPTH (ft)	OUTLET CONTROL DEPTH (ft)	FLOW TYPE <F4>	NORMAL DEPTH (ft)	CRIT. DEPTH (ft)	OUTLET DEPTH (ft)	TW DEPTH (ft)	OUTLET VEL. (fps)	TW VEL. (fps)
0.00	446.00	0.00	8.00	0-NF	0.00	0.00	0.00	8.10	0.00	0.00
6.00	446.04	1.09	8.04	4-FFt	0.91	0.80	2.50	8.10	1.22	0.00
12.00	446.17	1.69	8.17	4-FFt	1.36	1.16	2.50	8.10	2.44	0.00
18.00	446.39	2.17	8.39	4-FFt	1.79	1.43	2.50	8.10	3.67	0.00
24.00	446.69	2.64	8.69	4-FFt	2.50	1.66	2.50	8.10	4.89	0.00
30.00	447.08	3.16	9.08	4-FFt	2.50	1.86	2.50	8.10	6.11	0.00
36.00	447.55	3.80	9.55	4-FFt	2.50	2.03	2.50	8.10	7.33	0.00
42.00	448.11	4.56	10.11	4-FFt	2.50	2.15	2.50	8.10	8.56	0.00
45.00	448.43	4.99	10.43	4-FFt	2.50	2.22	2.50	8.10	9.17	0.00
54.00	449.49	6.47	11.49	4-FFt	2.50	2.41	2.50	8.10	11.00	0.00
60.00	450.31	7.61	12.31	4-FFt	2.50	2.50	2.50	8.10	12.22	0.00

El. inlet face invert           438.00 ft   El. outlet invert           437.90 ft  
 El. inlet throat invert        0.00 ft     El. inlet crest             0.00 ft

\*\*\*\*\* SITE DATA \*\*\*\*\* CULVERT INVERT \*\*\*\*\*  
 INLET STATION   0.00 ft  
 INLET ELEVATION                                        438.00 ft  
 OUTLET STATION   46.00 ft  
 OUTLET ELEVATION                                      437.90 ft  
 NUMBER OF BARRELS                                     1  
 SLOPE (V/H)    0.0022  
 CULVERT LENGTH ALONG SLOPE                         46.00 ft

\*\*\*\*\* CULVERT DATA SUMMARY \*\*\*\*\*  
 BARREL SHAPE   CIRCULAR  
 BARREL DIAMETER                                     2.50 ft  
 BARREL MATERIAL                                     CONCRETE  
 BARREL MANNING'S n                                 0.012  
 INLET TYPE   CONVENTIONAL  
 INLET EDGE AND WALL                                 SQUARE EDGE WITH HEADWALL  
 INLET DEPRESSION                                    NONE



CURRENT DATE: 01-08-2001  
CURRENT TIME: 16:30:03

FILE DATE: 01-08-2001  
FILE NAME: CAS

---

---

TAILWATER

---

---

CONSTANT WATER SURFACE ELEVATION  
446.00

---

---

ROADWAY OVERTOPPING DATA

---

---

ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH	12.00 ft
CREST LENGTH	50.00 ft
OVERTOPPING CREST ELEVATION	449.00 ft

---

**APPENDIX "E"**  
**BASIN VOLUMES**

---

## BASIN VOLUMES

### Lake A

Elevation	Surface Area	Stage Volume (cubic feet)	Accumulated Volume (cubic feet)	Remarks
447	3,804			Pool
448	4,934	4,369	4,369	
449	6,129	5,532	9,900	
450	6,970	6,549	16,450	
<b>Total</b>			<b>0.377 ac/ft</b>	

### Lake B

Elevation	Surface Area	Stage Volume (cubic feet)	Accumulated Volume (cubic feet)	Remarks
447	4,685			Pool
448	5,976	5,330	5,330	
449	7,272	6,624	11,954	
450	7,841	7,556	19,510	
<b>Total</b>			<b>0.447 ac/ft</b>	

### Lake C

Elevation	Surface Area	Stage Volume (cubic feet)	Accumulated Volume (cubic feet)	Remarks
445.50	3,049			Pool
446	4,759	1,952	1,952	
447	7,370	5,974	7,926	
448	11,636	9,503	17,429	
449	12,632	12,134	29,563	
<b>Total</b>			<b>0.677 ac/ft</b>	

### Lake D

Elevation	Surface Area	Stage Volume (cubic feet)	Accumulated Volume (cubic feet)	Remarks
445.50	18,731			Pool
446	22,830	10,390	10,390	
447	26,934	24,883	35,273	
448	31,047	28,990	64,263	
449	35,161	33,104	97,367	
<b>Total</b>			<b>2.235 ac/ft</b>	

## BASIN VOLUMES

### Lake E

Elevation	Surface Area	Stage Volume (cubic feet)	Accumulated Volume (cubic feet)	Remarks
445.50	4,356			Pool
446	5,337	2,423	2,423	
447	7,156	6,246	8,669	
448	8,948	8,052	16,721	
<b>Total</b>			<b>0.3839 ac/ft</b>	

### Lake F

Elevation	Surface Area	Stage Volume (cubic feet)	Accumulated Volume (cubic feet)	Remarks
444	5,862			Pool
445	7,588	6,725	6,725	
446	9,354	9,436	16,161	
447	11,284	10,319	26,480	
<b>Total</b>			<b>0.60 ac/ft</b>	

### Lake G

Elevation	Surface Area	Stage Volume (cubic feet)	Accumulated Volume (cubic feet)	Remarks
444	19,676			Pool
445	25,071	22,373	22,373	
446	30,103	27,587	49,960	
447	38,659	34,381	84,341	
<b>Total</b>			<b>1.936 ac/ft</b>	

Total storage available in ponds = 6.65 acre/feet

**APPENDIX "F"**

**STORMWATER ANALYSIS**

---



Job File: S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW  
Rain Dir: C:\HAESTAD\PPKW\RAINFALL\

=====  
JOB TITLE  
=====

POST DEVELOPED  
CASTLE CREEK

S/N: E21401D06A86 Bernardin Lochmueller & Associates  
PondPack Ver: 7.0 (325) Compute Time: 12:54:49 Date: 01-08-2001

Appendix F

Table of Contents

\*\*\*\*\* NETWORK SUMMARIES \*\*\*\*\*

Watershed..... 100 YR  
 Executive Summary (Nodes) ..... 1.01

\*\*\*\*\* DESIGN STORMS SUMMARY \*\*\*\*\*

Evil Storms... Design Storms ..... 2.01

\*\*\*\*\* POND VOLUMES \*\*\*\*\*

P-A..... Vol: Elev-Area ..... 3.01  
 P-B..... Vol: Elev-Area ..... 3.02  
 P-C..... Vol: Elev-Area ..... 3.03  
 P-D..... Vol: Elev-Area ..... 3.04  
 P-E..... Vol: Elev-Area ..... 3.05  
 P-F..... Vol: Elev-Area ..... 3.06  
 P-G..... Vol: Elev-Area ..... 3.07

\*\*\*\*\* OUTLET STRUCTURES \*\*\*\*\*

PR-AB..... Outlet Input Data ..... 4.01  
 Composite Rating Curve ..... 4.03  
 PR-BC..... Outlet Input Data ..... 4.10  
 Composite Rating Curve ..... 4.12

## Table of Contents (continued)

PR-CD.....	Outlet Input Data .....	4.22
	Composite Rating Curve .....	4.25
PR-DE.....	Outlet Input Data .....	4.33
	Composite Rating Curve .....	4.36
PR-EG.....	Outlet Input Data .....	4.42
	Composite Rating Curve .....	4.44
PR-FG.....	Outlet Input Data .....	4.52
	Composite Rating Curve .....	4.54
PR-OUT.....	Outlet Input Data .....	4.61
	Composite Rating Curve .....	4.64

## \*\*\*\*\* POND ROUTING \*\*\*\*\*

P-A.....	100 YR ICPM Node Routing Summary .....	5.01
P-B.....	100 YR ICPM Node Routing Summary .....	5.02
P-C.....	100 YR ICPM Node Routing Summary .....	5.03
P-D.....	100 YR ICPM Node Routing Summary .....	5.04
P-E.....	100 YR ICPM Node Routing Summary .....	5.05
P-F.....	100 YR ICPM Node Routing Summary .....	5.06
P-G.....	100 YR ICPM Node Routing Summary .....	5.07

Type.... Executive Summary (Nodes)  
 Name.... Watershed  
 File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW  
 Storm... 3rd Qrt Eville Tag: 100 YR

Page 1.01  
 Event: 100 yr

NETWORK SUMMARY -- NODES  
 (Trun.= HYG Truncation: Blank=None; L=Left; R=Rt; LR=Left & Rt)

DEFAULT Design Storm File, ID = HUFF.RNQ Eville Storms

Storm Tag Name = 100 YR  
 Description: Evansville Huff 100yr

-----  
 Data Type, File, ID = Synthetic Storm HUFF.RNF 3rd Qrt Eville  
 Storm Frequency = 100 yr  
 Total Rainfall Depth= 6.5200 in  
 Duration Multiplier = 1  
 Resulting Duration = 24.0000 hrs  
 Resulting Start Time= .0000 hrs Step= 1.2000 hrs End= 24.0000 hrs

-----  
 ICPM CALCULATION TOLERANCES

-----  
 Target Convergence= .000 cfs +/-  
 Max. Iterations = 35 loops  
 ICPM Time Step = .0500 hrs  
 Output Time Step = .0500 hrs  
 ICPM Ending Time = 35.0000 hrs  
 -----

Node ID	Type	HYG Vol ac-ft	Trun.	Qpeak hrs	Qpeak cfs	Max WSEL ft
AREA A	AREA	1.016		16.5500	1.15	
AREA B	AREA	.285		16.1500	.32	
AREA C	AREA	3.560		16.6500	4.04	
AREA D	AREA	9.019		16.8000	10.24	
AREA E	AREA	.427		16.7000	.49	
AREA F	AREA	1.358		16.7000	1.54	
AREA G	AREA	1.828		16.4500	2.07	
EAST OFFSITE	AREA	10.297		16.8000	13.30	
Outfall OUTLET	T-E	30.015	R	13.6500	37.11	446.50
P-A	POND	3.252		16.8000	4.29	
P-A	OUT POND	3.252		16.8000	4.23	448.90
P-B	POND	3.536		16.8000	4.55	
P-B	OUT POND	3.536		16.8500	4.50	448.63
P-C	POND	17.393		16.8000	21.83	
P-C	OUT POND	17.413		16.8000	21.67	448.39
P-D	POND	26.432		16.8000	31.90	
P-D	OUT POND	26.415	R	16.9000	31.57	448.06
P-E	POND	26.842	R	16.8500	32.02	
P-E	OUT POND	26.840	R	16.9000	31.97	447.40
P-F	POND	1.358		16.7000	1.54	
P-F	OUT POND	1.430	R	13.7000	3.43	446.31
P-F	OUT POND	-.075	R	13.1000	-3.80 (-Q)	

S/N: E21401D06A86 Bernardin Lochmueller & Associates  
 PondPack Ver: 7.0 (325) Compute Time: 12:54:49

Date: 01-08-2001

NETWORK SUMMARY -- NODES

(Trun.= HYG Truncation: Blank=None; L=Left; R=Rt; LR=Left & Rt)

Node ID	Type	HYG Vol ac-ft	Trun.	Qpeak hrs	Qpeak cfs	Max WSEL ft
P-G	POND	30.023	R	16.8000	35.52	
P-G	OUT POND	30.015	R	13.6500	37.11	446.33
SOUTH OFFSITE	AREA	2.236		16.8000	3.14	

Type.... Design Storms  
Name.... Eville Storms

Page 2.01

File.... C:\HAESTAD\PPKW\RAINFALL\HUFF.RNQ  
Title... POST DEVELOPED  
CASTLE CREEK

DESIGN STORMS SUMMARY

Design Storm File, ID = HUFF.RNQ      Eville Storms

Storm Tag Name      = 100 YR  
Description: Evansville Huff 100yr

-----  
Data Type, File, ID = Synthetic Storm HUFF.RNF 3rd Qrt Eville  
Storm Frequency      = 100 yr  
Total Rainfall Depth= 6.5200 in  
Duration Multiplier = 1  
Resulting Duration   = 24.0000 hrs  
Resulting Start Time= .0000 hrs   Step= 1.2000 hrs   End= 24.0000 hrs

S/N: E21401D06A86    Bernardin Lochmueller & Associates  
PondPack Ver: 7.0 (325)      Compute Time: 12:54:49

Date: 01-08-2001

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

Elevation (ft)	Planimeter (sq.in)	Area (acres)	A1+A2+sqr(A1*A2) (acres)	Volume (ac-ft)	Volume Sum (ac-ft)
447.00	-----	.0873	.0000	.000	.000
448.00	-----	.1133	.3000	.100	.100
449.00	-----	.1407	.3802	.127	.227
450.00	-----	.1600	.4507	.150	.377

POND VOLUME EQUATIONS

\* Incremental volume computed by the Conic Method for Reservoir Volumes.

$$\text{Volume} = (1/3) * (\text{EL2}-\text{EL1}) * (\text{Area1} + \text{Area2} + \text{sq.rt.}(\text{Area1}*\text{Area2}))$$

where: EL1, EL2 = Lower and upper elevations of the increment  
Area1,Area2 = Areas computed for EL1, EL2, respectively  
Volume = Incremental volume between EL1 and EL2



File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

Elevation (ft)	Planimeter (sq.in)	Area (acres)	A1+A2+sqr(A1*A2) (acres)	Volume (ac-ft)	Volume Sum (ac-ft)
447.00	-----	.1076	.0000	.000	.000
448.00	-----	.1372	.3662	.122	.122
449.00	-----	.1669	.4555	.152	.274
450.00	-----	.1800	.5203	.173	.447

POND VOLUME EQUATIONS

\* Incremental volume computed by the Conic Method for Reservoir Volumes.

$$\text{Volume} = (1/3) * (\text{EL2}-\text{EL1}) * (\text{Area1} + \text{Area2} + \text{sq.rt.}(\text{Area1}*\text{Area2}))$$

where: EL1, EL2 = Lower and upper elevations of the increment  
Area1,Area2 = Areas computed for EL1, EL2, respectively  
Volume = Incremental volume between EL1 and EL2

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

Elevation (ft)	Planimeter (sq. in)	Area (acres)	A1+A2+sqr(A1*A2) (acres)	Volume (ac-ft)	Volume Sum (ac-ft)
445.50	-----	.0700	.0000	.000	.000
446.00	-----	.1093	.2667	.044	.044
447.00	-----	.1692	.4144	.138	.183
448.00	-----	.2671	.6489	.216	.399
449.00	-----	.2900	.8354	.278	.677
450.00	-----	.3000	.8850	.295	.972

POND VOLUME EQUATIONS

\* Incremental volume computed by the Conic Method for Reservoir Volumes.

$$\text{Volume} = (1/3) * (\text{EL2}-\text{EL1}) * (\text{Area1} + \text{Area2} + \text{sq.rt.}(\text{Area1}*\text{Area2}))$$

where: EL1, EL2 = Lower and upper elevations of the increment  
Area1,Area2 = Areas computed for EL1, EL2, respectively  
Volume = Incremental volume between EL1 and EL2

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

Elevation (ft)	Planimeter (sq.in)	Area (acres)	A1+A2+sqr(A1*A2) (acres)	Volume (ac-ft)	Volume Sum (ac-ft)
445.50	-----	.4300	.0000	.000	.000
446.00	-----	.5241	1.4289	.238	.238
447.00	-----	.6183	1.7117	.571	.809
448.00	-----	.7127	1.9949	.665	1.474
449.00	-----	.8072	2.2784	.759	2.233

POND VOLUME EQUATIONS

\* Incremental volume computed by the Conic Method for Reservoir Volumes.

$$\text{Volume} = (1/3) * (\text{EL2}-\text{EL1}) * (\text{Area1} + \text{Area2} + \text{sq.rt.}(\text{Area1}*\text{Area2}))$$

where: EL1, EL2 = Lower and upper elevations of the increment  
Area1,Area2 = Areas computed for EL1, EL2, respectively  
Volume = Incremental volume between EL1 and EL2

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

Elevation (ft)	Planimeter (sq.in)	Area (acres)	A1+A2+sqr(A1*A2) (acres)	Volume (ac-ft)	Volume Sum (ac-ft)
445.50	-----	.1000	.0000	.000	.000
446.00	-----	.1225	.3332	.056	.056
447.00	-----	.1643	.4287	.143	.198
448.00	-----	.2054	.5534	.184	.383

POND VOLUME EQUATIONS

\* Incremental volume computed by the Conic Method for Reservoir Volumes.

$$\text{Volume} = (1/3) * (\text{EL2}-\text{EL1}) * (\text{Area1} + \text{Area2} + \text{sq.rt.}(\text{Area1}*\text{Area2}))$$

where: EL1, EL2 = Lower and upper elevations of the increment  
Area1,Area2 = Areas computed for EL1, EL2, respectively  
Volume = Incremental volume between EL1 and EL2

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

Elevation (ft)	Planimeter (sq. in)	Area (acres)	A1+A2+sqr(A1*A2) (acres)	Volume (ac-ft)	Volume Sum (ac-ft)
444.00	-----	.1346	.0000	.000	.000
445.00	-----	.1742	.4619	.154	.154
446.00	-----	.2147	.5823	.194	.348
447.00	-----	.2590	.7096	.237	.585

POND VOLUME EQUATIONS

\* Incremental volume computed by the Conic Method for Reservoir Volumes.

$$\text{Volume} = (1/3) * (\text{EL2}-\text{EL1}) * (\text{Area1} + \text{Area2} + \text{sq.rt.}(\text{Area1}*\text{Area2}))$$

where: EL1, EL2 = Lower and upper elevations of the increment  
Area1, Area2 = Areas computed for EL1, EL2, respectively  
Volume = Incremental volume between EL1 and EL2

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

Elevation (ft)	Planimeter (sq. in)	Area (acres)	A1+A2+sqr(A1*A2) (acres)	Volume (ac-ft)	Volume Sum (ac-ft)
444.00	-----	.4517	.0000	.000	.000
445.00	-----	.5756	1.5371	.512	.512
446.00	-----	.6911	1.8973	.632	1.145
447.00	-----	.8875	2.3617	.787	1.932

POND VOLUME EQUATIONS

\* Incremental volume computed by the Conic Method for Reservoir Volumes.

$$\text{Volume} = (1/3) * (\text{EL2}-\text{EL1}) * (\text{Area1} + \text{Area2} + \text{sq.rt.}(\text{Area1}*\text{Area2}))$$

where: EL1, EL2 = Lower and upper elevations of the increment  
Area1,Area2 = Areas computed for EL1, EL2, respectively  
Volume = Incremental volume between EL1 and EL2

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

REQUESTED POND WS ELEVATIONS:

Min. Elev.= 447.00 ft  
Increment = .50 ft  
Max. Elev.= 450.00 ft

OUTLET  
POND "A"  
STR No —  
18"  $\phi$  PIPE

\*\*\*\*\*

OUTLET CONNECTIVITY

\*\*\*\*\*

---> Forward Flow Only (UpStream to DnStream)  
<--- Reverse Flow Only (DnStream to UpStream)  
<---> Forward and Reverse Both Allowed

Structure	No.	Outfall	E1, ft	E2, ft
----- Culvert-Circular TW SETUP, DS Channel	CV	<---> TW	447.000	450.000

OUTLET STRUCTURE INPUT DATA

Structure ID = CV  
Structure Type = Culvert-Circular  
-----  
No. Barrels = 1  
Barrel Diameter = 1.5000 ft  
Upstream Invert = 447.00 ft  
Dnstream Invert = 447.00 ft  
Horiz. Length = 36.00 ft  
Barrel Length = 36.00 ft  
Barrel Slope = .00000 ft/ft

OUTLET CONTROL DATA...

Mannings n = .0120  
Ke = .0000 (forward entrance loss)  
Kb = .015519 (per ft of full flow)  
Kr = .0000 (reverse entrance loss)  
HW Convergence = .001 +/- ft

INLET CONTROL DATA...

Equation form = 1  
Inlet Control K = .0098  
Inlet Control M = 2.0000  
Inlet Control c = .03980  
Inlet Control Y = .6700  
T1 ratio (HW/D) = 1.160  
T2 ratio (HW/D) = 1.307  
Slope Factor = -.500

Use unsubmerged inlet control Form 1 equ. below T1 elev.  
Use submerged inlet control Form 1 equ. above T2 elev.

In transition zone between unsubmerged and submerged inlet control,  
interpolate between flows at T1 & T2...

At T1 Elev = 448.74 ft ---> Flow = 7.58 cfs  
At T2 Elev = 448.96 ft ---> Flow = 8.66 cfs



File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
447.00	.00	447.00	.000	None contributing
447.50	.76	447.00	.000	CV
448.00	3.04	447.00	.000	CV
448.50	6.19	447.00	.000	CV
449.00	8.83	447.00	.000	CV
449.50	10.83	447.00	.000	CV
450.00	12.51	447.00	.000	CV

Type.... Composite Rating Curve  
Name.... PR-AB

Page 4.04

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
447.00	-.76	447.50	.000	CV
447.50	.00	447.50	.000	CV
448.00	3.04	447.50	.000	CV
448.50	6.19	447.50	.000	CV
449.00	8.83	447.50	.000	CV
449.50	10.83	447.50	.000	CV
450.00	12.51	447.50	.000	CV

S/N: E21401D06A86 Bernardin Löchmueller & Associates  
PondPack Ver: 7.0 (325)

Compute Time: 12:54:49

Date: 01-08-2001

Type.... Composite Rating Curve  
Name.... PR-AB

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
447.00	-3.04	448.00	.000	CV
447.50	-3.04	448.00	.000	CV
448.00	.00	448.00	.000	CV
448.50	6.17	448.00	.000	CV
449.00	8.83	448.00	.000	CV
449.50	10.83	448.00	.000	CV
450.00	12.51	448.00	.000	CV

Type.... Composite Rating Curve  
Name.... PR-AB

Page 4.06

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
447.00	-6.19	448.50	.000	CV
447.50	-6.19	448.50	.000	CV
448.00	-6.18	448.50	.000	CV
448.50	.00	448.50	.000	CV
449.00	8.02	448.50	.000	CV
449.50	10.83	448.50	.000	CV
450.00	12.51	448.50	.000	CV

S/N: E21401D06A86 Bernardin Lochmueller & Associates  
PondPack Ver: 7.0 (325) Compute Time: 12:54:49

Date: 01-08-2001

Type.... Composite Rating Curve  
Name.... PR-AB

Page 4.07

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
447.00	-9.24	449.00	.000	CV
447.50	-9.24	449.00	.000	CV
448.00	-9.24	449.00	.000	CV
448.50	-8.03	449.00	.000	CV
449.00	.00	449.00	.000	CV
449.50	8.03	449.00	.000	CV
450.00	11.35	449.00	.000	CV

S/N: E21401D06A86 Bernardin Lochmueller & Associates  
PondPack Ver: 7.0 (325)

Compute Time: 12:54:49

Date: 01-08-2001

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
447.00	-11.80	449.50	.000	CV
447.50	-11.80	449.50	.000	CV
448.00	-11.80	449.50	.000	CV
448.50	-11.35	449.50	.000	CV
449.00	-8.03	449.50	.000	CV
449.50	.00	449.50	.000	CV
450.00	8.03	449.50	.000	CV

Type.... Composite Rating Curve  
Name.... PR-AB

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
447.00	-14.11	450.00	.000	CV
447.50	-14.11	450.00	.000	CV
448.00	-14.11	450.00	.000	CV
448.50	-13.91	450.00	.000	CV
449.00	-11.35	450.00	.000	CV
449.50	-8.03	450.00	.000	CV
450.00	.00	450.00	.000	CV

REQUESTED POND WS ELEVATIONS:

Min. Elev.= 447.00 ft  
Increment = .50 ft  
Max. Elev.= 450.00 ft

Pond B  
OUTLET STR -  
WEIR WALL

\*\*\*\*\*  
OUTLET CONNECTIVITY  
\*\*\*\*\*

- > Forward Flow Only (UpStream to DnStream)
- <--- Reverse Flow Only (DnStream to UpStream)
- <---> Forward and Reverse Both Allowed

Structure	No.	Outfall	E1, ft	E2, ft
Weir-Rectangular	W1 <--->	TW	447.000	450.000
Weir-Rectangular	W2 <--->	TW	448.500	450.000
TW SETUP, DS Channel				



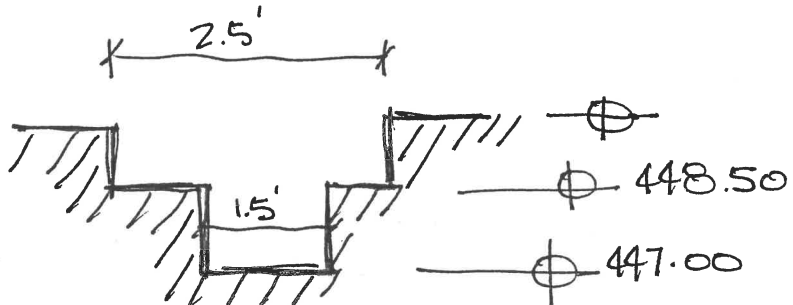
OUTLET STRUCTURE INPUT DATA

Structure ID = W1  
Structure Type = Weir-Rectangular  
-----  
# of Openings = 1  
Crest Elev. = 447.00 ft  
Weir Length = 1.50 ft  
Weir Coeff. = 3.320000

Weir TW effects (Use adjustment equation)

Structure ID = W2  
Structure Type = Weir-Rectangular  
-----  
# of Openings = 1  
Crest Elev. = 448.50 ft  
Weir Length = 2.50 ft  
Weir Coeff. = 3.000000

Weir TW effects (Use adjustment equation)



File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
447.00	.00	445.50	.000	W1
447.50	1.76	445.50	.000	W1
448.00	4.98	445.50	.000	W1
448.50	9.15	445.50	.000	W1 +W2
449.00	16.74	445.50	.000	W1 +W2
449.50	27.19	445.50	.000	W1 +W2
450.00	39.66	445.50	.000	W1 +W2

Type.... Composite Rating Curve  
Name.... PR-BC

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
447.00	.00	446.00	.000	W1
447.50	1.76	446.00	.000	W1
448.00	4.98	446.00	.000	W1
448.50	9.15	446.00	.000	W1 +W2
449.00	16.74	446.00	.000	W1 +W2
449.50	27.19	446.00	.000	W1 +W2
450.00	39.66	446.00	.000	W1 +W2

Type.... Composite Rating Curve  
Name.... PR-BC

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
447.00	.00	446.50	.000	W1
447.50	1.76	446.50	.000	W1
448.00	4.98	446.50	.000	W1
448.50	9.15	446.50	.000	W1 +W2
449.00	16.74	446.50	.000	W1 +W2
449.50	27.19	446.50	.000	W1 +W2
450.00	39.66	446.50	.000	W1 +W2

Type.... Composite Rating Curve  
Name.... PR-BC

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
447.00	.00	447.00	.000	W1
447.50	1.76	447.00	.000	W1
448.00	4.98	447.00	.000	W1
448.50	9.15	447.00	.000	W1 +W2
449.00	16.74	447.00	.000	W1 +W2
449.50	27.19	447.00	.000	W1 +W2
450.00	39.66	447.00	.000	W1 +W2

Type.... Composite Rating Curve  
Name.... PR-BC

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
447.00	-1.76	447.50	.000	W1
447.50	.00	447.50	.000	W1
448.00	4.21	447.50	.000	W1
448.50	8.43	447.50	.000	W1 +W2
449.00	16.03	447.50	.000	W1 +W2
449.50	26.49	447.50	.000	W1 +W2
450.00	38.96	447.50	.000	W1 +W2

Type.... Composite Rating Curve  
Name.... PR-BC

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
447.00	-4.98	448.00	.000	W1
447.50	-4.21	448.00	.000	W1
448.00	.00	448.00	.000	W1
448.50	6.76	448.00	.000	W1 +W2
449.00	14.56	448.00	.000	W1 +W2
449.50	25.09	448.00	.000	W1 +W2
450.00	37.61	448.00	.000	W1 +W2

Type.... Composite Rating Curve  
Name.... PR-BC

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
447.00	-9.15	448.50	.000	W1 +W2
447.50	-8.43	448.50	.000	W1 +W2
448.00	-6.76	448.50	.000	W1 +W2
448.50	.00	448.50	.000	W1 +W2
449.00	12.06	448.50	.000	W1 +W2
449.50	22.98	448.50	.000	W1 +W2
450.00	35.65	448.50	.000	W1 +W2



Type.... Composite Rating Curve  
Name.... PR-BC

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
447.00	-16.74	449.00	.000	W1 +W2
447.50	-16.03	449.00	.000	W1 +W2
448.00	-14.56	449.00	.000	W1 +W2
448.50	-12.06	449.00	.000	W1 +W2
449.00	.00	449.00	.000	W1 +W2
449.50	18.47	449.00	.000	W1 +W2
450.00	31.81	449.00	.000	W1 +W2

Type.... Composite Rating Curve  
Name.... PR-BC

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
447.00	-27.19	449.50	.000	W1 +W2
447.50	-26.49	449.50	.000	W1 +W2
448.00	-25.09	449.50	.000	W1 +W2
448.50	-22.98	449.50	.000	W1 +W2
449.00	-18.47	449.50	.000	W1 +W2
449.50	.00	449.50	.000	W1 +W2
450.00	25.10	449.50	.000	W1 +W2

Type.... Composite Rating Curve  
Name.... PR-BC

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
447.00	-39.66	450.00	.000	W1 +W2
447.50	-38.96	450.00	.000	W1 +W2
448.00	-37.61	450.00	.000	W1 +W2
448.50	-35.65	450.00	.000	W1 +W2
449.00	-31.81	450.00	.000	W1 +W2
449.50	-25.10	450.00	.000	W1 +W2
450.00	.00	450.00	.000	W1 +W2

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

REQUESTED POND WS ELEVATIONS:

Min. Elev.= 445.50 ft  
Increment = .50 ft  
Max. Elev.= 450.00 ft

\*\*\*\*\*  
OUTLET CONNECTIVITY  
\*\*\*\*\*

---> Forward Flow Only (UpStream to DnStream)  
<--- Reverse Flow Only (DnStream to UpStream)  
<---> Forward and Reverse Both Allowed

Structure	No.		Outfall	E1, ft	E2, ft
Culvert-Circular	CV	<--->	TW	445.500	450.000
Culvert-Circular	c2	--->	TW	445.500	450.000
TW SETUP, DS Channel					

OUTLET STRUCTURE INPUT DATA

Structure ID = CV  
Structure Type = Culvert-Circular  
-----  
No. Barrels = 1  
Barrel Diameter = 2.5000 ft  
Upstream Invert = 445.50 ft  
Dnstream Invert = 445.50 ft  
Horiz. Length = 36.00 ft  
Barrel Length = 36.00 ft  
Barrel Slope = .00000 ft/ft

← 30"  $\phi$  PIPE ←

OUTLET CONTROL DATA...

Mannings n = .0120  
Ke = .0000 (forward entrance loss)  
Kb = .007854 (per ft of full flow)  
Kr = .0000 (reverse entrance loss)  
HW Convergence = .001 +/- ft

INLET CONTROL DATA...

Equation form = 1  
Inlet Control K = .0098  
Inlet Control M = 2.0000  
Inlet Control c = .03980  
Inlet Control Y = .6700  
T1 ratio (HW/D) = 1.160  
T2 ratio (HW/D) = 1.307  
Slope Factor = -.500

Use unsubmerged inlet control Form 1 equ. below T1 elev.  
Use submerged inlet control Form 1 equ. above T2 elev.

In transition zone between unsubmerged and submerged inlet control,  
interpolate between flows at T1 & T2...

At T1 Elev = 448.40 ft ---> Flow = 27.16 cfs  
At T2 Elev = 448.77 ft ---> Flow = 31.05 cfs

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

OUTLET STRUCTURE INPUT DATA

Structure ID = c2  
Structure Type = Culvert-Circular  
-----  
No. Barrels = 1  
Barrel Diameter = 1.5000 ft  
Upstream Invert = 445.50 ft  
Dnstream Invert = 445.50 ft  
Horiz. Length = 36.00 ft  
Barrel Length = 36.00 ft  
Barrel Slope = .00000 ft/ft

← 18" Φ PIPE

OUTLET CONTROL DATA...

Mannings n = .0120  
Ke = .0000 (forward entrance loss)  
Kb = .015519 (per ft of full flow)  
Kr = .0000 (reverse entrance loss)  
HW Convergence = .001 +/- ft

INLET CONTROL DATA...

Equation form = 1  
Inlet Control K = .0098  
Inlet Control M = 2.0000  
Inlet Control c = .03980  
Inlet Control Y = .6700  
T1 ratio (HW/D) = 1.160  
T2 ratio (HW/D) = 1.307  
Slope Factor = -.500

Use unsubmerged inlet control Form 1 equ. below T1 elev.  
Use submerged inlet control Form 1 equ. above T2 elev.

In transition zone between unsubmerged and submerged inlet control,  
interpolate between flows at T1 & T2...

At T1 Elev = 447.24 ft ---> Flow = 7.58 cfs  
At T2 Elev = 447.46 ft ---> Flow = 8.66 cfs

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
445.50	.00	445.50	.000	None contributing
446.00	1.79	445.50	.000	CV +c2
446.50	7.39	445.50	.000	CV +c2
447.00	15.75	445.50	.000	CV +c2
447.50	24.86	445.50	.000	CV +c2
448.00	33.07	445.50	.000	CV +c2
448.50	40.73	445.50	.000	CV +c2
449.00	47.22	445.50	.000	CV +c2
449.50	52.85	445.50	.000	CV +c2
450.00	57.91	445.50	.000	CV +c2

Type.... Composite Rating Curve  
Name.... PR-CD

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
445.50	-1.04	446.00	.000	CV
446.00	.00	446.00	.000	CV +c2
446.50	7.39	446.00	.000	CV +c2
447.00	15.75	446.00	.000	CV +c2
447.50	24.86	446.00	.000	CV +c2
448.00	33.07	446.00	.000	CV +c2
448.50	40.73	446.00	.000	CV +c2
449.00	47.22	446.00	.000	CV +c2
449.50	52.85	446.00	.000	CV +c2
450.00	57.91	446.00	.000	CV +c2



Type.... Composite Rating Curve  
Name.... PR-CD

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
445.50	-4.35	446.50	.000	CV
446.00	-4.35	446.50	.000	CV
446.50	.00	446.50	.000	CV +c2
447.00	15.74	446.50	.000	CV +c2
447.50	24.86	446.50	.000	CV +c2
448.00	33.07	446.50	.000	CV +c2
448.50	40.73	446.50	.000	CV +c2
449.00	47.22	446.50	.000	CV +c2
449.50	52.85	446.50	.000	CV +c2
450.00	57.91	446.50	.000	CV +c2

Type.... Composite Rating Curve  
Name.... PR-CD

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
445.50	-9.56	447.00	.000	CV
446.00	-9.56	447.00	.000	CV
446.50	-9.56	447.00	.000	CV
447.00	.00	447.00	.000	CV +c2
447.50	23.92	447.00	.000	CV +c2
448.00	33.07	447.00	.000	CV +c2
448.50	40.73	447.00	.000	CV +c2
449.00	47.22	447.00	.000	CV +c2
449.50	52.85	447.00	.000	CV +c2
450.00	57.91	447.00	.000	CV +c2

Type.... Composite Rating Curve  
Name.... PR-CD

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
445.50	-16.16	447.50	.000	CV
446.00	-16.16	447.50	.000	CV
446.50	-16.16	447.50	.000	CV
447.00	-15.90	447.50	.000	CV
447.50	.00	447.50	.000	CV +c2
448.00	29.79	447.50	.000	CV +c2
448.50	39.57	447.50	.000	CV +c2
449.00	47.14	447.50	.000	CV +c2
449.50	52.85	447.50	.000	CV +c2
450.00	57.91	447.50	.000	CV +c2

Type.... Composite Rating Curve  
Name.... PR-CD

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
445.50	-23.56	448.00	.000	CV
446.00	-23.56	448.00	.000	CV
446.50	-23.56	448.00	.000	CV
447.00	-23.56	448.00	.000	CV
447.50	-21.74	448.00	.000	CV
448.00	.00	448.00	.000	CV +c2
448.50	32.61	448.00	.000	CV +c2
449.00	44.59	448.00	.000	CV +c2
449.50	51.42	448.00	.000	CV +c2
450.00	57.41	448.00	.000	CV +c2

Type.... Composite Rating Curve  
Name.... PR-CD

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
445.50	-31.09	448.50	.000	CV
446.00	-31.09	448.50	.000	CV
446.50	-31.09	448.50	.000	CV
447.00	-31.09	448.50	.000	CV
447.50	-30.97	448.50	.000	CV
448.00	-24.60	448.50	.000	CV
448.50	.00	448.50	.000	CV +c2
449.00	32.63	448.50	.000	CV +c2
449.50	46.12	448.50	.000	CV +c2
450.00	55.26	448.50	.000	CV +c2

Type.... Composite Rating Curve  
Name.... PR-CD

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
445.50	-37.98	449.00	.000	CV
446.00	-37.98	449.00	.000	CV
446.50	-37.98	449.00	.000	CV
447.00	-37.98	449.00	.000	CV
447.50	-37.98	449.00	.000	CV
448.00	-34.76	449.00	.000	CV
448.50	-24.60	449.00	.000	CV
449.00	.00	449.00	.000	CV +c2
449.50	32.61	449.00	.000	CV +c2
450.00	46.12	449.00	.000	CV +c2

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

REQUESTED POND WS ELEVATIONS:

Min. Elev.= 445.50 ft  
Increment = .50 ft  
Max. Elev.= 449.00 ft

Pond D

\*\*\*\*\*  
OUTLET CONNECTIVITY  
\*\*\*\*\*

---> Forward Flow Only (UpStream to DnStream)  
<--- Reverse Flow Only (DnStream to UpStream)  
<---> Forward and Reverse Both Allowed

Structure	No.		Outfall	E1, ft	E2, ft
Culvert-Circular	CV	<--->	TW	445.500	449.000
Culvert-Circular	c2	---	TW	445.500	449.000
TW SETUP, DS Channel					

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

OUTLET STRUCTURE INPUT DATA

Structure ID = CV  
Structure Type = Culvert-Circular  
-----  
No. Barrels = 1  
Barrel Diameter = 2.5000 ft  
Upstream Invert = 445.50 ft  
Dnstream Invert = 445.50 ft  
Horiz. Length = 37.00 ft  
Barrel Length = 37.00 ft  
Barrel Slope = .00000 ft/ft

← 30"

OUTLET CONTROL DATA...

Mannings n = .0120  
Ke = .0000 (forward entrance loss)  
Kb = .007854 (per ft of full flow)  
Kr = .0000 (reverse entrance loss)  
HW Convergence = .001 +/- ft

INLET CONTROL DATA...

Equation form = 1  
Inlet Control K = .0098  
Inlet Control M = 2.0000  
Inlet Control c = .03980  
Inlet Control Y = .6700  
T1 ratio (HW/D) = 1.160  
T2 ratio (HW/D) = 1.307  
Slope Factor = -.500

Use unsubmerged inlet control Form 1 equ. below T1 elev.  
Use submerged inlet control Form 1 equ. above T2 elev.

In transition zone between unsubmerged and submerged inlet control,  
interpolate between flows at T1 & T2...

At T1 Elev = 448.40 ft ---> Flow = 27.16 cfs  
At T2 Elev = 448.77 ft ---> Flow = 31.05 cfs



File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

OUTLET STRUCTURE INPUT DATA

Structure ID = c2  
Structure Type = Culvert-Circular

-----  
No. Barrels = 1  
Barrel Diameter = 1.5000 ft  
Upstream Invert = 445.50 ft  
Dnstream Invert = 445.50 ft  
Horiz. Length = 37.00 ft  
Barrel Length = 37.00 ft  
Barrel Slope = .00000 ft/ft

← 18"

OUTLET CONTROL DATA...

Mannings n = .0120  
Ke = .0000 (forward entrance loss)  
Kb = .015519 (per ft of full flow)  
Kr = .0000 (reverse entrance loss)  
HW Convergence = .001 +/- ft

INLET CONTROL DATA...

Equation form = 1  
Inlet Control K = .0098  
Inlet Control M = 2.0000  
Inlet Control c = .03980  
Inlet Control Y = .6700  
T1 ratio (HW/D) = 1.160  
T2 ratio (HW/D) = 1.307  
Slope Factor = -.500

Use unsubmerged inlet control Form 1 equ. below T1 elev.  
Use submerged inlet control Form 1 equ. above T2 elev.

In transition zone between unsubmerged and submerged inlet control,  
interpolate between flows at T1 & T2...

At T1 Elev = 447.24 ft ---> Flow = 7.58 cfs  
At T2 Elev = 447.46 ft ---> Flow = 8.66 cfs

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
445.50	.00	445.50	.000	None contributing
446.00	1.79	445.50	.000	CV +c2
446.50	7.36	445.50	.000	CV +c2
447.00	15.72	445.50	.000	CV +c2
447.50	24.86	445.50	.000	CV +c2
448.00	33.07	445.50	.000	CV +c2
448.50	40.73	445.50	.000	CV +c2
449.00	47.22	445.50	.000	CV +c2

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
445.50	-1.03	446.00	.000	CV
446.00	.00	446.00	.000	CV +c2
446.50	7.36	446.00	.000	CV +c2
447.00	15.72	446.00	.000	CV +c2
447.50	24.86	446.00	.000	CV +c2
448.00	33.07	446.00	.000	CV +c2
448.50	40.73	446.00	.000	CV +c2
449.00	47.22	446.00	.000	CV +c2

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
445.50	-4.34	446.50	.000	CV
446.00	-4.34	446.50	.000	CV
446.50	.00	446.50	.000	CV +c2
447.00	15.71	446.50	.000	CV +c2
447.50	24.86	446.50	.000	CV +c2
448.00	33.07	446.50	.000	CV +c2
448.50	40.73	446.50	.000	CV +c2
449.00	47.22	446.50	.000	CV +c2

Type.... Composite Rating Curve  
Name.... PR-DE

Page 4.39

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
445.50	-9.54	447.00	.000	CV
446.00	-9.54	447.00	.000	CV
446.50	-9.54	447.00	.000	CV
447.00	.00	447.00	.000	CV +c2
447.50	23.85	447.00	.000	CV +c2
448.00	33.07	447.00	.000	CV +c2
448.50	40.73	447.00	.000	CV +c2
449.00	47.22	447.00	.000	CV +c2

S/N: E21401D06A86 Bernardin Lochmueller & Associates  
PondPack Ver: 7.0 (325)

Compute Time: 12:54:49

Date: 01-08-2001

Type.... Composite Rating Curve  
Name.... PR-DE

Page 4.40

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
445.50	-16.12	447.50	.000	CV
446.00	-16.12	447.50	.000	CV
446.50	-16.12	447.50	.000	CV
447.00	-15.88	447.50	.000	CV
447.50	.00	447.50	.000	CV +c2
448.00	29.72	447.50	.000	CV +c2
448.50	39.52	447.50	.000	CV +c2
449.00	47.07	447.50	.000	CV +c2

S/N: E21401D06A86 Bernardin Lochmueller & Associates  
PondPack Ver: 7.0 (325) Compute Time: 12:54:49

Date: 01-08-2001

Type.... Composite Rating Curve  
Name.... PR-DE

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
445.50	-23.51	448.00	.000	CV
446.00	-23.51	448.00	.000	CV
446.50	-23.51	448.00	.000	CV
447.00	-23.51	448.00	.000	CV
447.50	-21.70	448.00	.000	CV
448.00	.00	448.00	.000	CV +c2
448.50	32.52	448.00	.000	CV +c2
449.00	44.53	448.00	.000	CV +c2

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

REQUESTED POND WS ELEVATIONS:

Min. Elev.= 445.50 ft  
Increment = .50 ft  
Max. Elev.= 448.00 ft

\*\*\*\*\*

OUTLET CONNECTIVITY

\*\*\*\*\*

- > Forward Flow Only (UpStream to DnStream)
- <--- Reverse Flow Only (DnStream to UpStream)
- <---> Forward and Reverse Both Allowed

Structure	No.		Outfall	E1, ft	E2, ft
-----	-----		-----	-----	-----
Weir-Rectangular	W1	<--->	TW	445.500	448.000
Weir-Rectangular	W2	<--->	TW	446.833	448.000
TW SETUP, DS Channel					



OUTLET STRUCTURE INPUT DATA

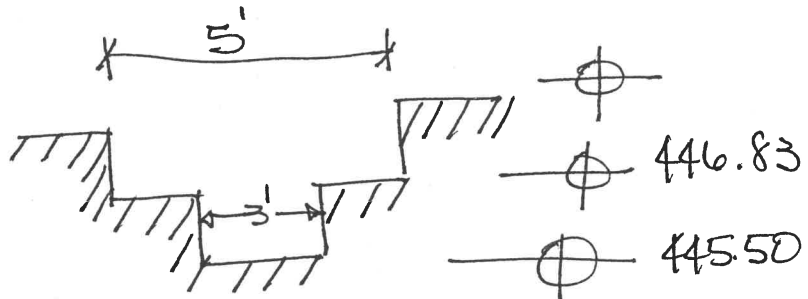
Structure ID = W1  
Structure Type = Weir-Rectangular  
-----  
# of Openings = 1  
Crest Elev. = 445.50 ft  
Weir Length = 3.00 ft  
Weir Coeff. = 3.320000

POUD E

Weir TW effects (Use adjustment equation)

Structure ID = W2  
Structure Type = Weir-Rectangular  
-----  
# of Openings = 1  
Crest Elev. = 446.83 ft  
Weir Length = 5.00 ft  
Weir Coeff. = 3.000000

Weir TW effects (Use adjustment equation)



File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge			Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures	
445.50	.00	444.00	.000	W1	
446.00	3.52	444.00	.000	W1	
446.50	9.96	444.00	.000	W1	
446.83	15.33	444.00	.000	W1 +W2	
447.00	19.32	444.00	.000	W1 +W2	
447.50	36.34	444.00	.000	W1 +W2	
448.00	58.28	444.00	.000	W1 +W2	

Type.... Composite Rating Curve  
Name.... PR-EG

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
445.50	.00	444.50	.000	W1
446.00	3.52	444.50	.000	W1
446.50	9.96	444.50	.000	W1
446.83	15.33	444.50	.000	W1 +W2
447.00	19.32	444.50	.000	W1 +W2
447.50	36.34	444.50	.000	W1 +W2
448.00	58.28	444.50	.000	W1 +W2

Type.... Composite Rating Curve  
Name.... PR-EG

Page 4.46

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
445.50	.00	445.00	.000	W1
446.00	3.52	445.00	.000	W1
446.50	9.96	445.00	.000	W1
446.83	15.33	445.00	.000	W1 +W2
447.00	19.32	445.00	.000	W1 +W2
447.50	36.34	445.00	.000	W1 +W2
448.00	58.28	445.00	.000	W1 +W2

S/N: E21401D06A86 Bernardin Lochmueller & Associates  
PondPack Ver: 7.0 (325) Compute Time: 12:54:49

Date: 01-08-2001

Type.... Composite Rating Curve  
Name.... PR-EG

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
445.50	.00	445.50	.000	W1
446.00	3.52	445.50	.000	W1
446.50	9.96	445.50	.000	W1
446.83	15.33	445.50	.000	W1 +W2
447.00	19.32	445.50	.000	W1 +W2
447.50	36.34	445.50	.000	W1 +W2
448.00	58.28	445.50	.000	W1 +W2

Type.... Composite Rating Curve  
Name.... PR-EG

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
445.50	-3.52	446.00	.000	W1
446.00	.00	446.00	.000	W1
446.50	8.42	446.00	.000	W1
446.83	13.86	446.00	.000	W1 +W2
447.00	17.88	446.00	.000	W1 +W2
447.50	34.93	446.00	.000	W1 +W2
448.00	56.89	446.00	.000	W1 +W2

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
445.50	-9.96	446.50	.000	W1
446.00	-8.42	446.50	.000	W1
446.50	.00	446.50	.000	W1
446.83	10.24	446.50	.000	W1 +W2
447.00	14.54	446.50	.000	W1 +W2
447.50	31.99	446.50	.000	W1 +W2
448.00	54.10	446.50	.000	W1 +W2

Type.... Composite Rating Curve  
Name.... PR-EG

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
445.50	-15.33	446.83	.000	W1 +W2
446.00	-13.86	446.83	.000	W1 +W2
446.50	-10.24	446.83	.000	W1 +W2
446.83	.00	446.83	.000	W1 +W2
447.00	10.11	446.83	.000	W1 +W2
447.50	28.99	446.83	.000	W1 +W2
448.00	51.47	446.83	.000	W1 +W2



Type.... Composite Rating Curve  
Name.... PR-EG

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
445.50	-19.32	447.00	.000	W1 +W2
446.00	-17.88	447.00	.000	W1 +W2
446.50	-14.54	447.00	.000	W1 +W2
446.83	-10.11	447.00	.000	W1 +W2
447.00	.00	447.00	.000	W1 +W2
447.50	26.58	447.00	.000	W1 +W2
448.00	49.46	447.00	.000	W1 +W2

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

REQUESTED POND WS ELEVATIONS:

Min. Elev.= 444.00 ft  
Increment = .50 ft  
Max. Elev.= 447.00 ft

POND F

\*\*\*\*\*  
OUTLET CONNECTIVITY  
\*\*\*\*\*

- > Forward Flow Only (UpStream to DnStream)
- <--- Reverse Flow Only (DnStream to UpStream)
- <---> Forward and Reverse Both Allowed

Structure	No.	Outfall	E1, ft	E2, ft
Culvert-Circular TW SETUP, DS Channel	CV	<---> TW	444.000	447.000

OUTLET STRUCTURE INPUT DATA

Structure ID = CV  
Structure Type = Culvert-Circular  
-----  
No. Barrels = 1  
Barrel Diameter = 2.0000 ft  
Upstream Invert = 444.00 ft  
Dnstream Invert = 444.00 ft  
Horiz. Length = 44.00 ft  
Barrel Length = 44.00 ft  
Barrel Slope = .00000 ft/ft

← 24"?

OUTLET CONTROL DATA...

Mannings n = .0120  
Ke = .0000 (forward entrance loss)  
Kb = .010575 (per ft of full flow)  
Kr = .0000 (reverse entrance loss)  
HW Convergence = .001 +/- ft

INLET CONTROL DATA...

Equation form = 1  
Inlet Control K = .0098  
Inlet Control M = 2.0000  
Inlet Control c = .03980  
Inlet Control Y = .6700  
T1 ratio (HW/D) = 1.160  
T2 ratio (HW/D) = 1.307  
Slope Factor = -.500

Use unsubmerged inlet control Form 1 equ. below T1 elev.  
Use submerged inlet control Form 1 equ. above T2 elev.

In transition zone between unsubmerged and submerged inlet control,  
interpolate between flows at T1 & T2...

At T1 Elev = 446.32 ft ---> Flow = 15.55 cfs  
At T2 Elev = 446.61 ft ---> Flow = 17.77 cfs

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Notes		
Elev. ft	Q cfs	TW Elev ft	Converge Error +/-ft	Contributing Structures
444.00	.00	444.00	.000	None contributing
444.50	.88	444.00	.000	CV
445.00	3.66	444.00	.000	CV
445.50	7.91	444.00	.000	CV
446.00	12.73	444.00	.000	CV
446.50	16.91	444.00	.000	CV
447.00	20.29	444.00	.000	CV

Type.... Composite Rating Curve  
Name.... PR-FG

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
444.00	-.88	444.50	.000	CV
444.50	.00	444.50	.000	CV
445.00	3.66	444.50	.000	CV
445.50	7.91	444.50	.000	CV
446.00	12.73	444.50	.000	CV
446.50	16.91	444.50	.000	CV
447.00	20.29	444.50	.000	CV

Type.... Composite Rating Curve  
Name.... PR-FG

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
444.00	-3.67	445.00	.000	CV
444.50	-3.67	445.00	.000	CV
445.00	.00	445.00	.000	CV
445.50	7.91	445.00	.000	CV
446.00	12.73	445.00	.000	CV
446.50	16.91	445.00	.000	CV
447.00	20.29	445.00	.000	CV

Type.... Composite Rating Curve  
Name.... PR-FG

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
444.00	-7.90	445.50	.000	CV
444.50	-7.90	445.50	.000	CV
445.00	-7.90	445.50	.000	CV
445.50	.00	445.50	.000	CV
446.00	12.51	445.50	.000	CV
446.50	16.91	445.50	.000	CV
447.00	20.29	445.50	.000	CV

Type.... Composite Rating Curve  
Name.... PR-FG

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge			Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures	
444.00	-12.95	446.00	.000	CV	
444.50	-12.95	446.00	.000	CV	
445.00	-12.95	446.00	.000	CV	
445.50	-12.49	446.00	.000	CV	
446.00	.00	446.00	.000	CV	
446.50	14.73	446.00	.000	CV	
447.00	20.29	446.00	.000	CV	



Type.... Composite Rating Curve  
Name.... PR-FG

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
444.00	-17.95	446.50	.000	CV
444.50	-17.95	446.50	.000	CV
445.00	-17.95	446.50	.000	CV
445.50	-17.95	446.50	.000	CV
446.00	-14.73	446.50	.000	CV
446.50	.00	446.50	.000	CV
447.00	14.72	446.50	.000	CV

Type.... Composite Rating Curve  
Name.... PR-FG

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
444.00	-22.26	447.00	.000	CV
444.50	-22.26	447.00	.000	CV
445.00	-22.26	447.00	.000	CV
445.50	-22.26	447.00	.000	CV
446.00	-20.81	447.00	.000	CV
446.50	-14.73	447.00	.000	CV
447.00	.00	447.00	.000	CV

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

REQUESTED POND WS ELEVATIONS:

Min. Elev.= 444.00 ft  
Increment = .50 ft  
Max. Elev.= 447.00 ft

POND G  
OUTFALL

\*\*\*\*\*  
OUTLET CONNECTIVITY  
\*\*\*\*\*

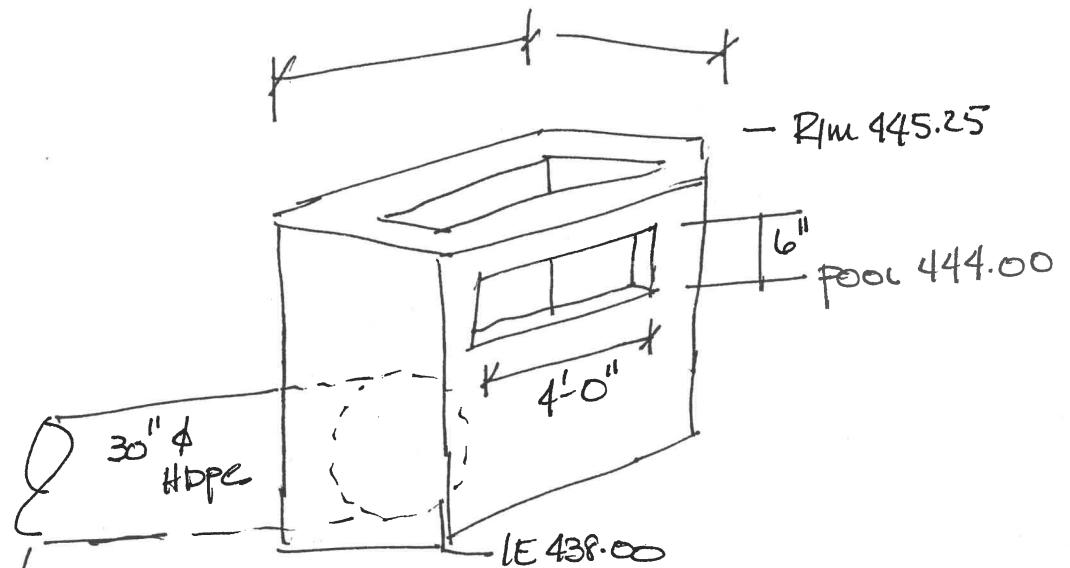
----> Forward Flow Only (UpStream to DnStream)  
<---- Reverse Flow Only (DnStream to UpStream)  
<----> Forward and Reverse Both Allowed

Structure	No.		Outfall	E1, ft	E2, ft
Inlet Box	BX	---->	CV	445.250	447.000
Orifice-Area	OR	---->	CV	444.000	447.000
Culvert-Circular	CV	---->	TW	438.000	447.000
TW SETUP, DS Channel					

OUTLET STRUCTURE INPUT DATA

Structure ID = BX  
Structure Type = Inlet Box  
-----  
# of Openings = 1  
Invert Elev. = 445.25 ft  
Orifice Area = 12.5000 sq.ft  
Orifice Coeff. = .600  
Weir Length = 15.00 ft  
Weir Coeff. = 3.000  
K, Submerged = .000  
K, Reverse = 1.000  
Kb, Barrel = .000000 (per ft of full flow)  
Barrel Length = .00 ft  
Mannings n = .0000

Structure ID = OR  
Structure Type = Orifice-Area  
-----  
# of Openings = 1  
Invert Elev. = 444.00 ft  
Area = 2.0000 sq.ft  
Top of Orifice = 444.50 ft  
Datum Elev. = 444.00 ft  
Orifice Coeff. = .600



IE 437.90

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

OUTLET STRUCTURE INPUT DATA

Structure ID = CV  
Structure Type = Culvert-Circular  
-----  
No. Barrels = 1  
Barrel Diameter = 2.5000 ft  
Upstream Invert = 438.00 ft  
Dnstream Invert = 437.90 ft  
Horiz. Length = 57.00 ft  
Barrel Length = 57.00 ft  
Barrel Slope = .00175 ft/ft

OUTLET CONTROL DATA...

Mannings n = .0150  
Ke = .0000 (forward entrance loss)  
Kb = .012271 (per ft of full flow)  
Kr = .0000 (reverse entrance loss)  
HW Convergence = .100 +/- ft

INLET CONTROL DATA...

Equation form = 1  
Inlet Control K = .0098  
Inlet Control M = 2.0000  
Inlet Control c = .03980  
Inlet Control Y = .6700  
T1 ratio (HW/D) = 1.159  
T2 ratio (HW/D) = 1.306  
Slope Factor = -.500

Use unsubmerged inlet control Form 1 equ. below T1 elev.  
Use submerged inlet control Form 1 equ. above T2 elev.

In transition zone between unsubmerged and submerged inlet control,  
interpolate between flows at T1 & T2...

At T1 Elev = 440.90 ft ---> Flow = 27.16 cfs  
At T2 Elev = 441.26 ft ---> Flow = 31.05 cfs

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Notes		
Elev. ft	Q cfs	TW Elev ft	Converge Error +/-ft	Contributing Structures
444.00	.00	437.00	.000	(no Q: BX,OR,CV)
444.50	6.81	437.00	.000	OR,CV (no Q: BX)
445.00	9.63	437.00	.000	OR,CV (no Q: BX)
445.25	10.76	437.00	.000	OR,CV (no Q: BX)
445.50	17.41	437.00	.000	BX,OR,CV
446.00	42.84	437.00	.000	BX,OR,CV
446.50	64.09	437.00	.000	BX,CV (no Q: OR)
447.00	66.38	437.00	.000	BX,CV (no Q: OR)

Type.... Composite Rating Curve  
Name.... PR-OUT

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
444.00	.00	437.90	.000	(no Q: BX,OR,CV)
444.50	6.81	437.90	.000	OR,CV (no Q: BX)
445.00	9.63	437.90	.000	OR,CV (no Q: BX)
445.25	10.76	437.90	.000	OR,CV (no Q: BX)
445.50	17.41	437.90	.000	BX,OR,CV
446.00	42.84	437.90	.000	BX,OR,CV
446.50	64.09	437.90	.000	BX,CV (no Q: OR)
447.00	66.38	437.90	.000	BX,CV (no Q: OR)

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
444.00	.00	438.00	.000	(no Q: BX,OR,CV)
444.50	6.81	438.00	.000	OR,CV (no Q: BX)
445.00	9.63	438.00	.000	OR,CV (no Q: BX)
445.25	10.76	438.00	.000	OR,CV (no Q: BX)
445.50	17.41	438.00	.000	BX,OR,CV
446.00	42.84	438.00	.000	BX,OR,CV
446.50	64.09	438.00	.000	BX,CV (no Q: OR)
447.00	66.38	438.00	.000	BX,CV (no Q: OR)



Type.... Composite Rating Curve  
Name.... PR-OUT

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
444.00	.00	439.00	.000	(no Q: BX,OR,CV)
444.50	6.81	439.00	.000	OR,CV (no Q: BX)
445.00	9.63	439.00	.000	OR,CV (no Q: BX)
445.25	10.76	439.00	.000	OR,CV (no Q: BX)
445.50	17.41	439.00	.000	BX,OR,CV
446.00	42.84	439.00	.000	BX,OR,CV
446.50	64.09	439.00	.000	BX,CV (no Q: OR)
447.00	66.38	439.00	.000	BX,CV (no Q: OR)

Type.... Composite Rating Curve  
Name.... PR-OUT

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
444.00	.00	440.00	.000	(no Q: BX,OR,CV)
444.50	6.81	440.00	.000	OR,CV (no Q: BX)
445.00	9.63	440.00	.000	OR,CV (no Q: BX)
445.25	10.76	440.00	.000	OR,CV (no Q: BX)
445.50	17.41	440.00	.000	BX,OR,CV
446.00	42.84	440.00	.000	BX,OR,CV
446.50	64.09	440.00	.000	BX,CV (no Q: OR)
447.00	66.38	440.00	.000	BX,CV (no Q: OR)

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
444.00	.00	441.00	.000	(no Q: BX,OR,CV)
444.50	6.81	441.00	.000	OR,CV (no Q: BX)
445.00	9.63	441.00	.000	OR,CV (no Q: BX)
445.25	10.76	441.00	.000	OR,CV (no Q: BX)
445.50	17.41	441.00	.000	BX,OR,CV
446.00	42.84	441.00	.000	BX,OR,CV
446.50	64.09	441.00	.000	BX,CV (no Q: OR)
447.00	66.38	441.00	.000	BX,CV (no Q: OR)

Type.... Composite Rating Curve  
Name.... PR-OUT

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .004 (+/- ft)  
FLOW PATH: Elev= 446; Branch: OR-CV-TW

\* Max. convergence errors shown may also occur for  
flow paths other than the ones listed above.

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
444.00	.00	442.00	.000	(no Q: BX,OR,CV)
444.50	6.81	442.00	.000	OR,CV (no Q: BX)
445.00	9.63	442.00	.000	OR,CV (no Q: BX)
445.25	10.76	442.00	.000	OR,CV (no Q: BX)
445.50	17.41	442.00	.000	BX,OR,CV
446.00	42.80	442.00	.004	BX,OR,CV
446.50	63.59	442.00	.000	BX,CV (no Q: OR)
447.00	66.38	442.00	.000	BX,CV (no Q: OR)

Type.... Composite Rating Curve  
Name.... PR-OUT

Page 4.71

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .008 (+/- ft)  
FLOW PATH: Elev= 446; Branch: OR-CV-TW

\* Max. convergence errors shown may also occur for  
flow paths other than the ones listed above.

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
444.00	.00	443.00	.000	(no Q: BX,OR,CV)
444.50	6.81	443.00	.000	OR,CV (no Q: BX)
445.00	9.63	443.00	.000	OR,CV (no Q: BX)
445.25	10.76	443.00	.000	OR,CV (no Q: BX)
445.50	17.41	443.00	.000	BX,OR,CV
446.00	39.96	443.00	.008	BX,OR,CV
446.50	56.08	443.00	.000	BX,CV (no Q: OR)
447.00	60.15	443.00	.000	BX,CV (no Q: OR)

S/N: E21401D06A86 Bernardin Lochmueller & Associates  
PondPack Ver: 7.0 (325)

Compute Time: 12:54:49

Date: 01-08-2001

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .008 (+/- ft)  
FLOW PATH: Elev= 445.5; Branch: OR-CV-TW

\* Max. convergence errors shown may also occur for  
flow paths other than the ones listed above.

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
444.00	.00	444.00	.000	(no Q: BX,OR,CV)
444.50	6.45	444.00	.005	OR,CV (no Q: BX)
445.00	9.18	444.00	.001	OR,CV (no Q: BX)
445.25	10.26	444.00	.001	OR,CV (no Q: BX)
445.50	16.25	444.00	.008	BX,OR,CV
446.00	36.34	444.00	.000	BX,CV (no Q: OR)
446.50	48.07	444.00	.000	BX,CV (no Q: OR)
447.00	51.86	444.00	.000	BX,CV (no Q: OR)

Type.... Composite Rating Curve  
Name.... PR-OUT

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .007 (+/- ft)  
FLOW PATH: Elev= 445.5; Branch: OR-CV-TW

\* Max. convergence errors shown may also occur for  
flow paths other than the ones listed above.

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
444.00	.00	445.00	.000	(no Q: BX,OR,CV)
444.50	.00	445.00	.000	(no Q: BX,OR,CV)
445.00	.00	445.00	.000	(no Q: BX,OR,CV)
445.25	4.56	445.00	.003	OR,CV (no Q: BX)
445.50	11.43	445.00	.007	BX,OR,CV
446.00	30.90	445.00	.000	BX,CV (no Q: OR)
446.50	36.05	445.00	.000	BX,CV (no Q: OR)
447.00	43.56	445.00	.000	BX,CV (no Q: OR)

Type.... Composite Rating Curve  
Name.... PR-OUT

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
444.00	.00	445.25	.000	(no Q: BX,OR,CV)
444.50	.00	445.25	.000	(no Q: BX,OR,CV)
445.00	.00	445.25	.000	(no Q: BX,OR,CV)
445.25	.00	445.25	.000	(no Q: BX,OR,CV)
445.50	14.88	445.25	.000	BX,CV (no Q: OR)
446.00	27.04	445.25	.000	BX,CV (no Q: OR)
446.50	34.05	445.25	.000	BX,CV (no Q: OR)
447.00	39.41	445.25	.000	BX,CV (no Q: OR)



\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
444.00	.00	446.00	.000	(no Q: BX,OR,CV)
444.50	.00	446.00	.000	(no Q: BX,OR,CV)
445.00	.00	446.00	.000	(no Q: BX,OR,CV)
445.25	.00	446.00	.000	(no Q: BX,OR,CV)
445.50	.00	446.00	.000	(no Q: BX,OR,CV)
446.00	.00	446.00	.000	(no Q: BX,OR,CV)
446.50	20.03	446.00	.000	BX,CV (no Q: OR)
447.00	29.04	446.00	.000	BX,CV (no Q: OR)

Type.... Composite Rating Curve  
Name.... PR-OUT

File.... S:\HAESTAD\PROJECTS\CASTLECREEK197-181\POST\_DEVELOP\_EGCHK.PPW

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

CUMULATIVE HGL CONVERGENCE ERROR .000 (+/- ft)

WS Elev, Total Q		Converge		Notes
Elev. ft	Q cfs	TW Elev ft	Error +/-ft	Contributing Structures
444.00	.00	447.00	.000	(no Q: BX,OR,CV)
444.50	.00	447.00	.000	(no Q: BX,OR,CV)
445.00	.00	447.00	.000	(no Q: BX,OR,CV)
445.25	.00	447.00	.000	(no Q: BX,OR,CV)
445.50	.00	447.00	.000	(no Q: BX,OR,CV)
446.00	.00	447.00	.000	(no Q: BX,OR,CV)
446.50	.00	447.00	.000	(no Q: BX,OR,CV)
447.00	.00	447.00	.000	(no Q: BX,OR,CV)

ICPM POND ROUTING SUMMARY

HYG Dir = S:\HAESTAD\PROJECTS\CASTLECREEK197-181\  
 Inflow HYG file = P-A IN 100 YR  
 Outflow HYG file = P-A OUT 100 YR

Pond Node Data = P-A  
 Pond Volume Data = P-A  
 Pond Outlet Data = PR-AB

No Infiltration

INITIAL CONDITIONS

-----  
 Starting WS Elev = 447.00 ft  
 Starting Volume = .000 ac-ft  
 Starting Outflow = .00 cfs  
 -----

CALCULATION TOLERANCES

-----  
 Target Convergence= .000 cfs +/-  
 Max. Iterations = 35 loops  
 ICPM Time Step = .0500 hrs  
 Output Time Step = .0500 hrs  
 ICPM Ending Time = 35.0000 hrs  
 -----

MAXIMUM STORAGE

Tp, hrs	Elev, ft	Vol, ac-ft
-----		
16.9000	448.90	.214

FORWARD FLOW PEAKS

Tp, hrs	Qp, cfs
-----	

Pond Inflow.....	16.8000	4.29
Pond Outflow....	16.8000	4.23

REVERSE FLOW PEAKS

Tp, hrs	Qp, cfs
-----	

	.0000	.00
	.0000	.00

TOTAL VOLUME IN

Vol, ac-ft	Direction
-----	

Pond Inflow.....	3.252	Forward
Pond Outflow....	.000	Reverse

TOTAL VOLUME OUT

Vol, ac-ft	Direction
-----	

	.000	Reverse
	3.252	Forward

MASS BALANCE (ac-ft)

+ Initial Vol.....	.000	
+ Total Vol IN....	3.252	
- Total Vol OUT...	3.252	
- Ending Pond Vol.	.000	<-- (At 35.0000 hrs Elev.= 447.00 ft)
-----		
Difference.....	.000 ac-ft	(.004% of Inflow Volume)

ICPM POND ROUTING SUMMARY

HYG Dir = S:\HAESTAD\PROJECTS\CASTLECREEK197-181\  
 Inflow HYG file = P-B IN 100 YR  
 Outflow HYG file = P-B OUT 100 YR

Pond Node Data = P-B  
 Pond Volume Data = P-B  
 Pond Outlet Data = PR-BC

No Infiltration

INITIAL CONDITIONS

-----  
 Starting WS Elev = 447.00 ft  
 Starting Volume = .000 ac-ft  
 Starting Outflow = .00 cfs  
 -----

CALCULATION TOLERANCES

-----  
 Target Convergence= .000 cfs +/-  
 Max. Iterations = 35 loops  
 ICPM Time Step = .0500 hrs  
 Output Time Step = .0500 hrs  
 ICPM Ending Time = 35.0000 hrs  
 -----

MAXIMUM STORAGE

Tp, hrs	Elev, ft	Vol, ac-ft
-----		
16.9000	448.63	.218

FORWARD FLOW PEAKS

Tp, hrs	Qp, cfs
-----	

REVERSE FLOW PEAKS

Tp, hrs	Qp, cfs
-----	

Pond Inflow.....	16.8000	4.55	.0000	.00
Pond Outflow....	16.8500	4.50	.0000	.00

TOTAL VOLUME IN

Vol, ac-ft	Direction
-----	

TOTAL VOLUME OUT

Vol, ac-ft	Direction
-----	

Pond Inflow.....	3.536	Forward	.000	Reverse
Pond Outflow....	.000	Reverse	3.536	Forward

MASS BALANCE (ac-ft)

-----  
 + Initial Vol..... .000  
 + Total Vol IN.... 3.536  
 - Total Vol OUT... 3.536  
 - Ending Pond Vol. .000 <-- (At 35.0000 hrs Elev.= 447.00 ft)

-----  
 Difference..... - .000 ac-ft (.001% of Outflow Volume)

ICPM POND ROUTING SUMMARY

HYG Dir = S:\HAESTAD\PROJECTS\CASTLECREEK197-181\  
 Inflow HYG file = P-C IN 100 YR  
 Outflow HYG file = P-C OUT 100 YR

Pond Node Data = P-C  
 Pond Volume Data = P-C  
 Pond Outlet Data = PR-CD

No Infiltration

INITIAL CONDITIONS

-----  
 Starting WS Elev = 445.50 ft  
 Starting Volume = .000 ac-ft  
 Starting Outflow = .00 cfs  
 -----

CALCULATION TOLERANCES

-----  
 Target Convergence= .000 cfs +/-  
 Max. Iterations = 35 loops  
 ICPM Time Step = .0500 hrs  
 Output Time Step = .0500 hrs  
 ICPM Ending Time = 35.0000 hrs  
 -----

MAXIMUM STORAGE

Tp, hrs	Elev, ft	Vol, ac-ft
-----		
16.9000	448.39	.507

FORWARD FLOW PEAKS

Tp, hrs	Qp, cfs
-----	

Pond Inflow.....	16.8000	21.83
Pond Outflow....	16.8000	21.67

REVERSE FLOW PEAKS

Tp, hrs	Qp, cfs
-----	

	.0000	.00
	.0000	.00

TOTAL VOLUME IN  
Vol, ac-ft Direction

TOTAL VOLUME OUT  
Vol, ac-ft Direction

Pond Inflow.....	17.393	Forward		.000	Reverse
Pond Outflow....	.000	Reverse		17.413	Forward

MASS BALANCE (ac-ft)

-----  
 + Initial Vol..... .000  
 + Total Vol IN.... 17.393  
 - Total Vol OUT... 17.413  
 - Ending Pond Vol. .003 <-- (At 35.0000 hrs Elev.= 445.53 ft)

Difference..... -.022 ac-ft (.127% of Outflow Volume)

ICPM POND ROUTING SUMMARY

HYG Dir = S:\HAESTAD\PROJECTS\CASTLECREEK197-181\  
 Inflow HYG file = P-D IN 100 YR  
 Outflow HYG file = P-D OUT 100 YR

Pond Node Data = P-D  
 Pond Volume Data = P-D  
 Pond Outlet Data = PR-DE

No Infiltration

INITIAL CONDITIONS

-----  
 Starting WS Elev = 445.50 ft  
 Starting Volume = .000 ac-ft  
 Starting Outflow = .00 cfs  
 -----

CALCULATION TOLERANCES

-----  
 Target Convergence= .000 cfs +/-  
 Max. Iterations = 35 loops  
 ICPM Time Step = .0500 hrs  
 Output Time Step = .0500 hrs  
 ICPM Ending Time = 35.0000 hrs  
 -----

MAXIMUM STORAGE

Tp, hrs	Elev, ft	Vol, ac-ft
-----		
16.9000	448.06	1.522

FORWARD FLOW PEAKS

Tp, hrs	Qp, cfs
-----	

REVERSE FLOW PEAKS

Tp, hrs	Qp, cfs
-----	

Pond Inflow.....	16.8000	31.90	.0000	.00
Pond Outflow....	16.9000	31.57	.0000	.00

TOTAL VOLUME IN

Vol, ac-ft	Direction
-----	

TOTAL VOLUME OUT

Vol, ac-ft	Direction
-----	

Pond Inflow.....	26.432	Forward	.000	Reverse
Pond Outflow....	.000	Reverse	26.415	Forward

MASS BALANCE (ac-ft)

-----  
 + Initial Vol..... .000  
 + Total Vol IN.... 26.432  
 - Total Vol OUT... 26.415  
 - Ending Pond Vol. .015 <-- (At 35.0000 hrs Elev.= 445.53 ft)  
 -----  
 Difference..... .001 ac-ft (.004% of Inflow Volume)

ICPM POND ROUTING SUMMARY

HYG Dir = S:\HAESTAD\PROJECTS\CASTLECREEK197-181\  
 Inflow HYG file = P-E IN 100 YR  
 Outflow HYG file = P-E OUT 100 YR

Pond Node Data = P-E  
 Pond Volume Data = P-E  
 Pond Outlet Data = PR-EG

No Infiltration

INITIAL CONDITIONS

-----  
 Starting WS Elev = 445.50 ft  
 Starting Volume = .000 ac-ft  
 Starting Outflow = .00 cfs  
 -----

CALCULATION TOLERANCES

-----  
 Target Convergence= .000 cfs +/-  
 Max. Iterations = 35 loops  
 ICPM Time Step = .0500 hrs  
 Output Time Step = .0500 hrs  
 ICPM Ending Time = 35.0000 hrs  
 -----

MAXIMUM STORAGE

Tp, hrs	Elev, ft	Vol, ac-ft
-----		
16.9000	447.40	.272

FORWARD FLOW PEAKS

Tp, hrs	Qp, cfs
-----	

REVERSE FLOW PEAKS

Tp, hrs	Qp, cfs
-----	

Pond Inflow.....	16.8500	32.02	13.1000	.00
Pond Outflow....	16.9000	31.97	13.1000	.00

TOTAL VOLUME IN  
 Vol, ac-ft Direction

TOTAL VOLUME OUT  
 Vol, ac-ft Direction

Pond Inflow.....	26.842	Forward	.000	Reverse
Pond Outflow....	.000	Reverse	26.840	Forward

MASS BALANCE (ac-ft)

-----  
 + Initial Vol..... .000  
 + Total Vol IN.... 26.842  
 - Total Vol OUT... 26.840  
 - Ending Pond Vol. .002 <-- (At 35.0000 hrs Elev.= 445.51 ft)  
 -----  
 Difference..... .001 ac-ft (.002% of Inflow Volume)

ICPM POND ROUTING SUMMARY

HYG Dir = S:\HAESTAD\PROJECTS\CASTLECREEK197-181\  
 Inflow HYG file = P-F IN 100 YR  
 Outflow HYG file = P-F OUT 100 YR

Pond Node Data = P-F  
 Pond Volume Data = P-F  
 Pond Outlet Data = PR-FG

No Infiltration

INITIAL CONDITIONS

-----  
 Starting WS Elev = 444.00 ft  
 Starting Volume = .000 ac-ft  
 Starting Outflow = .00 cfs  
 -----

CALCULATION TOLERANCES

-----  
 Target Convergence= .000 cfs +/-  
 Max. Iterations = 35 loops  
 ICPM Time Step = .0500 hrs  
 Output Time Step = .0500 hrs  
 ICPM Ending Time = 35.0000 hrs  
 -----

MAXIMUM STORAGE

Tp, hrs	Elev, ft	Vol, ac-ft
-----		
13.3500	446.31	.422

FORWARD FLOW PEAKS

Tp, hrs	Qp, cfs
-----	

Pond Inflow.....	16.7000	1.54
Pond Outflow....	13.7000	3.43

REVERSE FLOW PEAKS

Tp, hrs	Qp, cfs
-----	

	.0000	.00
	13.1000	-3.80

TOTAL VOLUME IN

Vol, ac-ft	Direction
-----	

Pond Inflow.....	1.358	Forward
Pond Outflow....	.075	Reverse

TOTAL VOLUME OUT

Vol, ac-ft	Direction
-----	

	.000	Reverse
	1.430	Forward

MASS BALANCE (ac-ft)

-----  
 + Initial Vol..... .000  
 + Total Vol IN.... 1.433  
 - Total Vol OUT... 1.430  
 - Ending Pond Vol. .003 <-- (At 35.0000 hrs Elev.= 444.02 ft)  
 -----  
 Difference..... --.000 ac-ft (.003% of Inflow Volume)



ICPM POND ROUTING SUMMARY

HYG Dir = S:\HAESTAD\PROJECTS\CASTLECREEK197-181\  
 Inflow HYG file = P-G IN 100 YR  
 Outflow HYG file = P-G OUT 100 YR

Pond Node Data = P-G  
 Pond Volume Data = P-G  
 Pond Outlet Data = PR-OUT

No Infiltration

INITIAL CONDITIONS

-----  
 Starting WS Elev = 444.00 ft  
 Starting Volume = .000 ac-ft  
 Starting Outflow = .00 cfs  
 -----

CALCULATION TOLERANCES

-----  
 Target Convergence= .000 cfs +/-  
 Max. Iterations = 35 loops  
 ICPM Time Step = .0500 hrs  
 Output Time Step = .0500 hrs  
 ICPM Ending Time = 35.0000 hrs  
 -----

MAXIMUM STORAGE

Tp, hrs	Elev, ft	Vol, ac-ft
-----		
13.2000	446.33	1.406

FORWARD FLOW PEAKS

Tp, hrs	Qp, cfs
-----	

REVERSE FLOW PEAKS

Tp, hrs	Qp, cfs
-----	

Pond Inflow.....	16.8000	35.52	13.1000	.00
Pond Outflow....	13.6500	37.11	13.1000	.00

TOTAL VOLUME IN

Vol, ac-ft	Direction
-----	

TOTAL VOLUME OUT

Vol, ac-ft	Direction
-----	

Pond Inflow.....	30.023	Forward	.000	Reverse
Pond Outflow....	.000	Reverse	30.015	Forward

MASS BALANCE (ac-ft)

-----  
 + Initial Vol..... .000  
 + Total Vol IN.... 30.023  
 - Total Vol OUT... 30.015  
 - Ending Pond Vol. .005 <-- (At 35.0000 hrs Elev.= 444.01 ft)

-----  
 Difference..... .002 ac-ft (.008% of Inflow Volume)

## Index of Starting Page Numbers for ID Names

----- E -----

Eville Storms... 2.01

----- P -----

P-A... 3.01, 5.01

P-B... 3.02, 5.02

P-C... 3.03, 5.03

P-D... 3.04, 5.04

P-E... 3.05, 5.05

P-F... 3.06, 5.06

P-G... 3.07, 5.07

PR-AB... 4.01, 4.03

PR-BC... 4.10, 4.12

PR-CD... 4.22, 4.25

PR-DE... 4.33, 4.36

PR-EG... 4.42, 4.44

PR-FG... 4.52, 4.54

PR-OUT... 4.61, 4.64

----- W -----

Watershed 100 YR... 1.01