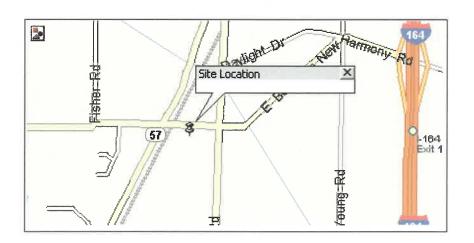
AMLIGHT FARM SUPPLY

## DRAINAGE REPORT

### **FOR**

## **Snyder Investments, LLC**

Site Location: 4505 Boonville-New Harmony Road Evansville, IN



Prepared By:

Hinderliter Construction, LLC
3601 North Saint Joseph Ave
Evansville, Indiana 47720

September 27, 2005

RECEIVED BY THE VAN ERBURGH COUNTY SURVEYOR'S OFFICE

9/28/05 1:28 pm AND



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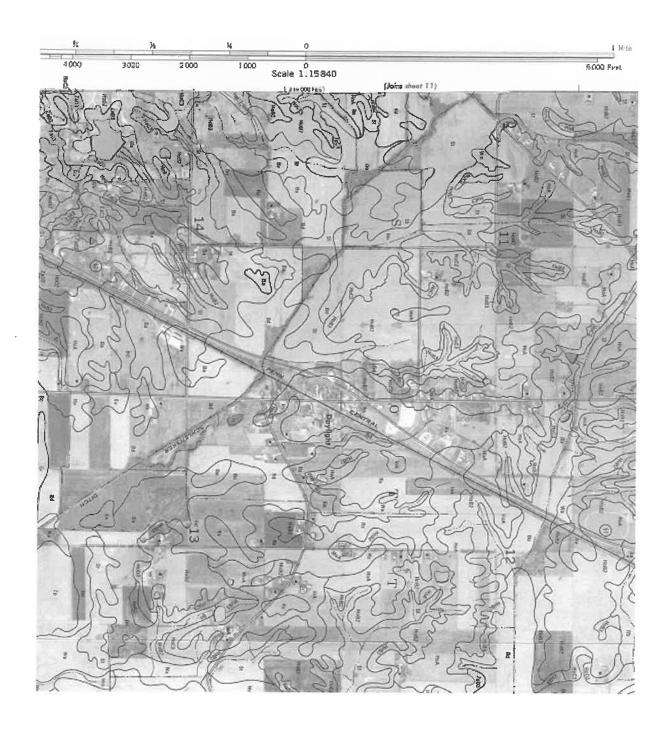
## Site Map



## **Aerial Photograph**



## Soils Map



#### **Existing Site Conditions**

The site is located on the south side of Boonville New Harmony Road approximately 700' west of the intersection of Green River Road and Boonville New Harmony Road.

The existing 5.22 acre site is comprised of generally flat terrain bounded on the north side by a roadside ditch. This ditch drains easterly to the roadside ditch at Green River Road. The site is bounded on the west by swale that drains northerly to a roadside. This ditch drains easterly to the roadside ditch at Green River. The site is bounded on the south and east by a drainage ditch that empties into the detention lake for Daylight Industrial Park.

According to the Soil Survey of Vanderburgh County Indiana, the site's soil is comprised of Birds Silt Loam and Wakeland Silt Loam.

Existing contours are indicated on the drawing attached. It should be noted that there were no previous structures or stone parking areas on this site. The site's current use is agricultural.

### **Proposed Improvements**

**Basin #1,** with regard to *developed* conditions, has a total area of 153,754 SF. The proposed improvements within Basin #1-Post include:

- 30,000 SF of new structure
- 22,788 SF of new concrete pavement
- 8,000 SF of water surface (when Dry Basin is full at spillway elevation)

Runoff from the building, paved drives, and parking area, will be directed via surface flow and grass swales to the dry basin structure.

#### **Drainage Calculations**

The Rational Method was utilized for the pre and post development drainage calculations. Calculations for pre-developed basins 1, 2, and 3, are attached. Each calculation sheet indicates the pre-developed runoff rate (in bold at the bottom of each respective page).

All pre-developed runoff calculations were performed with respect to a 10-year storm event frequency. Post-developed runoff calculations (for detention basin calculations) were performed with respect to a 25-year storm event frequency.

#### Pre-developed Basin Information (see attached Basin drawing):

**Basin "1"** is comprised of 153,754 SF of area. The existing contours indicate a drainage pattern northeasterly to a swale along the south side of Boonville New Harmony Road. The grade of this basin is less than 1% and is vegetated. This area has no "concentrated" outfall but would deliver approximately 2.24 CFS, under a 10 year storm event, to the roadside ditch.

**Basin "2"** is comprised of 50,062 SF of area. The existing contours indicate a drainage pattern northeasterly to a swale. The grade of this basin is less than 1% and is vegetated. This area has no "concentrated" outfall but would deliver approximately .97 CFS, under a 10 year storm event, to the drainage ditch emptying to the existing detention basin.

**Basin "3"** is comprised of 23,749 of area. The existing contours indicate a drainage pattern southeasterly to a ditch along the south property line. The grade of this basin is less than 1% and is vegetated. This area has no "concentrated" outfall but would deliver approximately 0.42 CFS, under a 10 year storm event, to the ditch.

Storm water detention will be provided within the subject site for the entire proposed improved area. All improvements in pre-developed Basin #1 and a portion of pre-developed basin #2 (where the building extends into Basin #2 4,757 SF) will be provided by constructing a dry basin feature along the north line of the property and releasing at the northeast corner of the site. The proposed basin will have a storage capacity of 8,400 CF at an average depth of 2.1'. This is 15% over the required capacity of 6,960 CF.

### UNDEVELOPED CALCULATIONS FLOW FOR A 10 YEAR STORM

l.											
	Job Name	: Svnder, I	Basin #1								
		9/27/20						153 754	Total SF	3.53 A	C.
ł								100,101	1010101	0.00 /	
	Impervious surface	es (2-5%)	C=0.94								
	Structures		0 Total	(	) SF			0	Total SF	0.00 A	С
	Drives		0 Total		) SF				Total SF	0.00 A	
	Pavement		0 Width (ft)		L (ft)				Total SF	0.00 A	
l,	Patios		0 Total		SF				Total SF	0.00 A	
	Sidewalks		0 Width (ft)		L (ft)				Total SF	0.00 A	
	Gravel, C=.75		0 Total		SF				Total SF	0.00 A	
	, , , , , , , , , , , , , , , , , , , ,								TOTAL	0.00 A	
								·	·OIAL	0.00 / 1	
	Lake (C=1.0)		0 Total	C	) SF			0	Total SF	0.00 A	C
								0	TOTAL	0.00 A	
	For cultivated field	s:									
	0-2% slope	C=0.20		138,379	SF			138,379	Total SF	3.18 A	0
	2-5% slope	C=0.35		C	SF			0	Total SF	0.00 A	0
	5-10% slope	C=0.50		C	SF			0	Total SF	0.00 A	2
	10+% slope	C=0.65		C	SF				Total SF	0.00 A	2_
								138,379	TOTAL	3.18 A	0
	Turf Lawns:										
	0-2% slope	C=0.15		15,375				15,375	Total SF	0.35 A	2
	2-5% slope	C=0.25			SF			0	Total SF	0.00 A	2
	5-10% slope	C=0.40		0	SF		_		Total SF	0.00 A	<u></u>
								15,375	TOTAL	0.35 A	3
	For woodland area										
	0-2% slope	C=0.12			SF				Total SF	0.00 AC	
	2-5% slope	C=0.24			SF				Total SF	0.00 AC	
	5-10% slope	C=0.36			SF				Total SF	0.00 AC	
	10+% slope	C=0.48		0	SF		9		Total SF	0.00 AC	_
								0	TOTAL	0.00 AC	)
							014	450 754		0.50.44	
			1441	0.00			CK.	153,754	GI	3.53 AC	;
			Wt'd C =	0.20							
			Wt'd N =	0.22							
			High Pt El	390.00							
			Inlet El	386.00							
			Length	720.00							
			Slope	0.0056							
			tc	29.61	min						
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	ı	U	19 20-10-01	J f	1 10-	0.00	11 1/ (1)				

### UNDEVELOPED CALCULATIONS FLOW FOR A 10 YEAR STORM

Job Name	Synder,	Basin #2								
Date	9/27/20	005					50,062	Total SF	1.15 A	С
lana e de la constante de la c	(0.50()	0.004								
Impervious surface	es (2-5%)			0.05			•			_
Structures Drives		0 Total		0 SF				Total SF	0.00 A	
Pavement		0 Total		OSF				Total SF	0.00 A	
Patios		0 Width (ft) 0 Total		0 L (ft)				Total SF	0.00 A	
Sidewalks		0 Width (ft)		OSF				Total SF	0.00 A	
Gravel, C=.75		0 Total		0 L (ft) 0 SF				Total SF	0.00 A	
Olavol, 070		0 Total	,	JOI		-		Total SF TOTAL	0.00 A	_
							U	IOIAL	0.00 A	_
Lake (C=1.0)		0 Total	(	) SF			0	Total SF	0.00 A	2
_							0	TOTAL	0.00 A	$\overline{z}$
For cultivated fields										
0-2% slope	C=0.20		50,062					Total SF	1.15 A	
2-5% slope	C=0.35			) SF				Total SF	0.00 A	
5-10% slope	C=0.50			) SF				Total SF	0.00 A	
10+% slope	C=0.65		(	) SF				Total SF	0.00 A	_
Turf Lawns:							50,062	TOTAL	1.15 A	)
0-2% slope	C=0.15		(	) SF			n	Total SF	0.00 A	-
2-5% slope	C=0.25			) SF				Total SF	0.00 A	
5-10% slope	C=0.40			) SF				Total SF	0.00 A	
-						3-		TOTAL	0.00 AC	_
For woodland area	s:									
0-2% slope	C=0.12		C	) SF			0	Total SF	0.00 AC	)
2-5% slope	C=0.24		C	SF			0	Total SF	0.00 AC	)
5-10% slope	C=0.36			) SF			0	Total SF	0.00 AC	)
10+% slope	C=0.48		C	SF				Total SF	0.00 AC	<u>)                                    </u>
							0	TOTAL	0.00 AC	)
					С	K.	50,062	GT	1.15 AC	)
		Wt'dC =	0.20	)						
		Wt'dN =	0.20	)						
		High Pt El	389.00	ft						
		Inlet El	386.00							
		Length	360.00							
		Slope	0.0083							
		tc	18.64	min						
0	1	ls 5 <tc<10< td=""><td>?</td><td>i 10=</td><td>0.00 in</td><td>/hr</td><td></td><td></td><td></td><td></td></tc<10<>	?	i 10=	0.00 in	/hr				
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1	0	Is 30 <tc<6< td=""><td>0?</td><td></td><td>0.00 in</td><td></td><td></td><td></td><td></td><td></td></tc<6<>	0?		0.00 in					

Q10= 0.97 cfs

### UNDEVELOPED CALCULATIONS FLOW FOR A 10 YEAR STORM

	01102112		2211101151	LOWI	OK II IU I EA	KSTOKM		
Job Name	: Synder, I : 9/27/20					22 760	Total CE	0.55.40
Date	. 3/2//20	05				23,769	Total SF	0.55 AC
Impervious surfac	es (2-5%)	C=0.94						
Structures		0 Total		0 SF		0	Total SF	0.00 AC
Drives		0 Total	(	0 SF		0	Total SF	0.00 AC
Pavement		0 Width (ft)		0 L (ft)		0	Total SF	0.00 AC
Patios		0 Total		0 SF		0	Total SF	0.00 AC
Sidewalks		0 Width (ft)		0 L (ft)			Total SF	0.00 AC
Gravel, C=.75		0 Total	(	0 SF			Total SF	0.00 AC
						0	TOTAL	0.00 AC
Lake (C=1.0)		0 Total	(	0 SF		0	Total SF	0.00 AC
						0	TOTAL	0.00 AC
For cultivated field			00.70	0.05		00.700	T	
0-2% slope	C=0.20		23,769			-	Total SF	0.55 AC
2-5% slope	C=0.35			0 SF			Total SF	0.00 AC
5-10% slope 10+% slope	C=0.50 C=0.65			0 SF 0 SF			Total SF	0.00 AC
101 % Slope	C-0.00		,	U SF	9		Total SF	0.00 AC
Turf Lawns:						23,769	TOTAL	0.55 AC
0-2% slope	C=0.15		(	0 SF		0	Total SF	0.00 AC
2-5% slope	C=0.25			0 SF			Total SF	0.00 AC
5-10% slope	C=0.40		(	) SF			Total SF	0.00 AC
•					,		TOTAL	0.00 AC
For woodland area								
0-2% slope	C=0.12			) SF			Total SF	0.00 AC
2-5% slope	C=0.24			) SF			Total SF	0.00 AC
5-10% slope	C=0.36			SF			Total SF	0.00 AC
10+% slope	C=0.48		(	) SF			Total SF	0.00 AC
						. 0	TOTAL	0.00 AC
					CK.	23,769	GT	0.55 AC
		Wt'd C =	0.20					
		Wt'd N =	0.20					
		High Pt El	390.00					
		Inlet El	386.00					
		Length	530.00					
		Slope	0.0075					
		tc	22.85	min o				
0	1	ls 5 <tc<10< td=""><td>?</td><td>i 10=</td><td>0.00 in/hr</td><td></td><td></td><td></td></tc<10<>	?	i 10=	0.00 in/hr			
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1	1	Is 15 <tc<3< td=""><td>0?</td><td>i 10=</td><td>3.84 in/hr</td><td></td><td></td><td></td></tc<3<>	0?	i 10=	3.84 in/hr			
1	0	ls 30 <tc<6< td=""><td>0?</td><td>i 10=</td><td>0.00 in/hr</td><td></td><td></td><td></td></tc<6<>	0?	i 10=	0.00 in/hr			

Q10= 0.42 cfs

## **DEVELOPED CALCULATIONS FLOW FOR A 25 YEAR STORM**

						O TEXTO OTTIM	
Job Name/Basin #:	Sovder	Rasin #1					
	9/27/20					153,754 Total SF	3.53 AC
Exist. Impervious s	urfaces (2	•					
Structures		0 Total		SF		0 Total SF	0.00 AC
Drives		0 Total		SF		0 Total SF	0.00 AC
Pavement		0 Width (ft)	0	L (ft)		0 Total SF	0.00 AC
						0 TOTAL	0.00 AC
Lake (C=1.0)		0 Total	0	SF		0 Total SF	0 AC
						0 TOTAL	0.00 AC
Proposed Impervio	us surfac	es (2-5%) C=	0.94				
Structures		1 Total	30,000	SF		30,000 Total SF	0.69 AC
Future Impervious		0 Total	0	SF		0 Total SF	0.00 AC
Pavement		1 Width (ft)	22,788	L (ft)		22,788 Total SF	0.52 AC
Patios		0 Total	0	SF		0 Total SF	0.00 AC
Sidewalks		0 Width (ft)	0	L (ft)		0 Total SF	0.00 AC
						52,788 <b>TOTAL</b>	1.21 AC
Lake (C=1.0)		1 Total	8000	SF		8000 Total SF	0.18 AC
(,			0000	O.		8,000 TOTAL	0.18 AC
Exist cultivated field	ds:					·	
0-2% slope	C=0.20		0	SF		0 Total SF	0.00 AC
2-5% slope	C=0.35		0	SF		0 Total SF	0.00 AC
5-10% slope	C=0.50		0	SF		0 Total SF	0.00 AC
10+% slope	C=0.65		0	SF		0 Total SF	0.00 AC
Trust I arras						0 TOTAL	0.00 AC
Turf Lawns	0 0 45			0.5			
0-2% slope	C=0.15		92,966			92,966 Total SF	2.13 AC
2-5% slope	C=0.25		0			0 Total SF	0.00 AC
5-10% slope	C=0.40			SF		0 Total SF	0.00 AC
10+% slope	C=0.55		Ü	SF		0 Total SF	0.00 AC
For woodland areas	2.					92,966 <b>TOTAL</b>	2.13 AC
	C=0.12		Ω	SF		0 Total SF	0.00 AC
	C=0.24			SF		0 Total SF	0.00 AC
•	C=0.36			SF		0 Total SF	0.00 AC
•	C=0.48			SF		0 Total SF	
10. 70 Glope	0-0.40		U	OI .	3	0 TOTAL	0.00 AC
						OTOTAL	0.00 AC
					Ck	153,754 <b>GT</b>	3.53 AC
		Wt'd C =	0.47				
		Wt'd N =	0.25				
		High Pt El	390.00				
		Inlet El	383.20	ft			
		1 41	00000	F1			

Length

Slope

tc

830.00 ft

30.66 min

0.0082

0 1	ls 5 <tc<10?< th=""><th>i 25=</th><th>0.00 in/hr</th></tc<10?<>	i 25=	0.00 in/hr
0 1	Is 10 <tc<15?< td=""><td>i 25=</td><td>0.00 in/hr</td></tc<15?<>	i 25=	0.00 in/hr
0 1	Is 15 <tc<30?< td=""><td>i 25=</td><td>0.00 in/hr</td></tc<30?<>	i 25=	0.00 in/hr
1 1	ls 30 <tc<60?< td=""><td>i 25=</td><td>3.61 in/hr</td></tc<60?<>	i 25=	3.61 in/hr

Q25= 5.93 cfs

#### **Detention Basin**

Pre-developed runoff rate (from 3.53 AC to the NE site corner) = 2.24 CFS

Post-developed runoff rate (from 3.53 AC to the NE site corner) = 5.93 CFS

The controlled post developed release rate will be at the pre-developed rate of 2.24 CFS. This will be accomplished through a 12" diameter pipe with 7.5". The orifice calculation is below:

### Orifice Calculation For Outlet Structure, Snyder Investments

#### **ORIFICE CALCULATIONS**

Q=Ca(2gh)^.5

Use 0.6 for "C" h=Head on CL of orifice

Q10=	2.24	cfs
C=	0.6	
g=	32.2	ft/sec2
h=	2.3	ft
a=	0.30675	sf
orifice radius =	0.31	ft
Diameter =	7.5	in

The outfall "structure" will consist of a rip-rap terrace to decrease outfall water velocity to protect against erosion.

## Vanderburgh County Drainage Board Form 800

## Computation Sheet for Detention Storage Using the Rational Method

Project: Snyder Date: 9/27/2005	
Detention Facility Design Return Period	25 years
Release Rate Return Period	10 years
Watershed Area	3.53 acres
Undeveloped Time of Concentration	29.6 minutes
Undeveloped Rainfall Intensity (iu)	3.26 inches/hour
Weighted Undeveloped Runoff Coefficient (Cu)	0.20
Undeveloped Runoff Rate (O=Cu x iu x Au)	2.24 cfs
Developed Runoff Coefficient (Cd)	0.47

Storm Duration td	Rainfall Intensity id	Inflow Rate I(td)	Outflow Rate O	Storage Rate	Required Storage
		Cd x id x Ad	Cu x iu x Au	(I x td) - O	[l(td)-O]x[td/12]
min	inches/hr	cfs	cfs	cfs	acre-ft
5	7.208	11.96	2.24	9.72	0.0675
10	5.925	9.83	2.24	7.59	0.1054
15	5.033	8.35	2.24	6.11	0.1273
20	4.571	7.58	2.24	5.34	0.1484
25	4.108	6.82	2.24	4.58	0.1589
30	3.646	6.05	2.24	3.81	0.1587
40	3.123	5.18	2.24	2.94	0.1634
50	2.601	4.32	2.24	2.08	0.1441
60	2.078	3.45	2.24	1.21	0.1006
90	1.578	2.62	2.24	0.38	0.0473
Req'd	Storage =	0.1589	x 43,560 sf/ac=	6,922	cubic feet

Proposed Storage Lake Area =

8,000.00 SF

Resulting Required Storage Depth =

0.87 Ft